#### DRAINAGE STATEMENT

For

#### NorthStar Capital, LLC

**Point View Luxury Apartments** 

Block 113, Lots 41 & 43 842 & 850 Arnold Avenue Borough of Point Pleasant, Ocean County, NJ

Prepared by:



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NJ Professional Engineer License #45896

December 2020 DEC # 3639-99-001

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#### **APPENDIX**

- Runoff Curve Number (CN) Calculations Existing
- Runoff Curve Number (CN) Calculations Proposed
- Hydrograph Summary Reports Existing & Proposed Conditions, 2 & 10 Yr. Storm Events
- Web Soil Survey Map
- Pipe Sizing Calculations
- Soil Testing Logs
- Drainage Area Maps

I. <u>DRAINAGE SUMMARY</u>

This Drainage Statement has been prepared to define and analyze the stormwater drainage conditions that

would occur as a result of the redevelopment of the existing dentist office and single-family home, located at

842 and 850 Arnold Avenue in the Borough of Point Pleasant, Ocean County, New Jersey.

Under the present conditions, the site is developed as an existing dentist office and single-family home. The

existing development has an impervious coverage of 12,693 SF (0.29 Acres). The proposed development is a

Multi-Family Apartment Complex with associated parking, landscaping, lighting, and other site amenities.

The proposed development's impervious coverage is 21,447 SF (0.49 Acres). The net increase in impervious

area is 8,754 SF (0.20 Acres).

This Drainage Statement identifies and describes the manner by which the design provides the performance

measures to minimize the adverse impact of stormwater runoff. As this project consists of less than one acre of

land disturbance and proposes less than ¼ acre increase in impervious surface, it does not qualify as a "major"

development, and is not subject to the new NJDEP stormwater management, water quality, or groundwater

recharge regulations (NJAC 7:8). Therefore, the study has been prepared to comply with the New Jersey Soil

Erosion and Sediment Control Standards for flow reduction requirements. The scope of the study includes the

construction of the proposed building, associated driveways and parking areas, landscaping, stormwater

collection system, and associated improvements as shown on the accompanying engineering drawings.

Hydrological evaluation is provided for the 2 and 10 year storm events utilizing the Urban Hydrology for

Small Watershed TR55 method. The TR55 method is utilized to design the detention system. The Rational

Method is used to size the storm drainage system.

The SCD flow reduction requirements are as follows:

2-year:

50% reduction of any increase in the existing impervious surface runoff

10-year:

25% reduction of any increase in the existing impervious surface runoff

II. EXISTING DRAINAGE CONDITIONS

The existing conditions of the tract have been verified by the Boundary and Topography Survey as prepared by

InSite Surveying, LLC, dated July 24, 2020, last revised August 12, 2020. This information has been utilized

to establish an Existing Conditions Drainage Area Map which is included within the Appendix of this Report.

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The tract has been evaluated with the following existing drainage sub-watershed area:

<u>Study Area South</u>: This area consists of the existing dentist office and single-family home with associated impervious and open space areas. Under existing conditions stormwater runoff from this area is tributary to the southern property line.

Based on Ocean County soils survey information, the soil types native to the site include:

	OCEAN COUNTY SOIL SURVEY INFORM	ATION
SOIL TYPE (SYMBOL)	SOIL TYPE (NAME)	HYDROLOGIC SOIL GROUP (HSG)
EveB	Evesboro sand, 0 to 5 percent slopes	A

#### III. PROPOSED DRAINAGE CONDITIONS

The proposed development includes the construction of a Multifamily Apartment Complex. Additional site improvements include paved parking areas, landscaping, lighting and other site amenities. The proposed stormwater management facilities, more specifically the proposed aboveground infiltration basin and underground infiltration basin with bubbler outlet have been designed to account for the additional stormwater runoff from the proposed development.

The tract has been evaluated with the following drainage sub-watershed areas as depicted on the Proposed Conditions Drainage Area Map:

<u>Study Area South:</u> This area of the tract consists of proposed paved area on the eastern side of the proposed building and landscaped areas that drain to the open area at the south of the site.

Study Area Basin A: This area of the tract consists of proposed paved area north of the proposed building and landscaped areas that drain to the proposed aboveground basin on the western side of the site. The proposed basin system serves to control the release of stormwater from the 2 & 10 year design storms through a spillway near the southern property line.

<u>Study Area Roof:</u> This area consists of the roof of the proposed building. Under proposed conditions stormwater runoff from this area is deposited into an underground infiltration basin. The proposed basin system detains both the 2 & 10 year design storms with any overflow for larger storms through a proposed bubbler inlet located along the southern property line.

#### IV. <u>DESIGN METHODOLOGY</u>

The intention of the design of the proposed stormwater management facility for this project is to provide measures as required to address applicable aspects of the Standards for Soil Erosion and Sediment Control in New Jersey.

The stormwater runoff conditions have been modeled utilizing the Hydraflow computer software based on the TR55 "Urban Hydrology for Small Watersheds" method of hydrologic design. The proposed aboveground infiltration basin and underground infiltration basin has been designed to meet the 2 and 10 year stormwater runoff rate reductions as required by the Standards for Soils Erosions and Sediment Control in New Jersey. The stormwater basins detain the stormwater runoff and releases the stormwater at a controlled rate through a spillway and bubbler inlet located at the southern property line.

#### VI. RUNOFF RATE REDUCTION PERFORMANCE

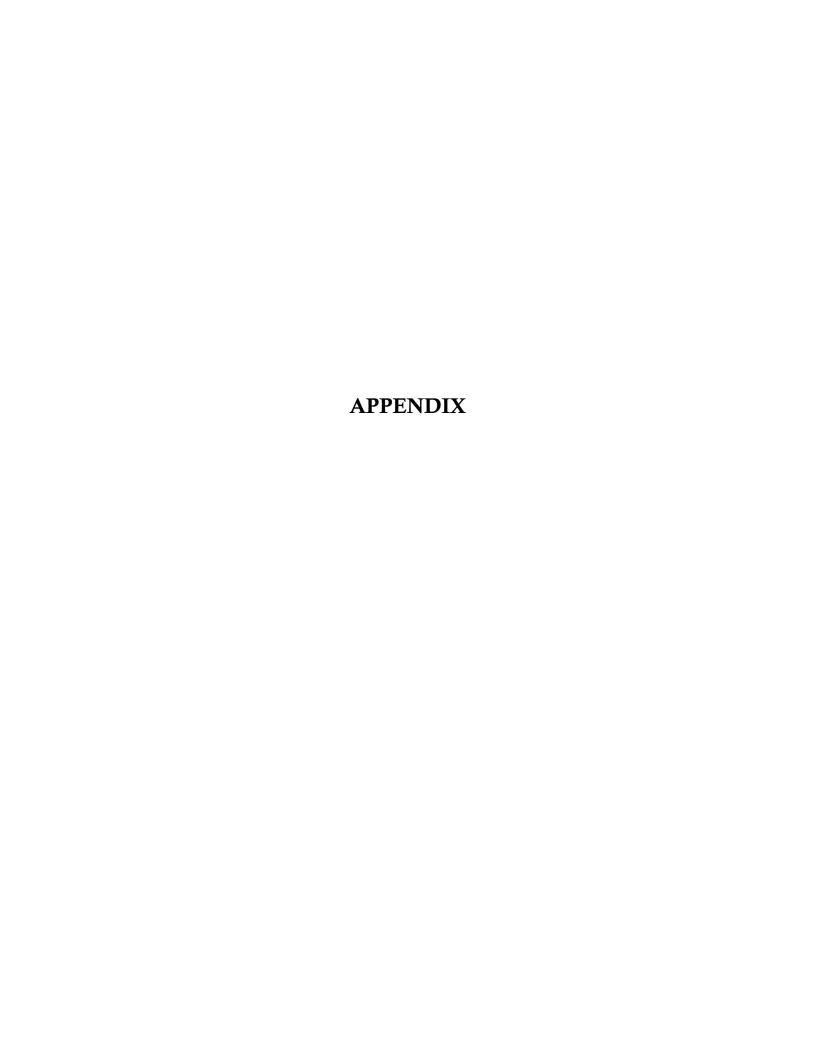
The proposed stormwater management system has been designed in accordance with Standards for Soils Erosions and Sediment Control in New Jersey. The aboveground system has been designed to ensure that the runoff reduction standards are achieved. Standards for Soils Erosions and Sediment Control in New Jersey requires that the proposed increase in runoff for the two (2) and the ten (10) year design storms modeled as 24-hour SCS Type III design storms must reduce the net increase of impervious coverage by 50% and 25%, respectively.

Design Storm	Overall Existing Runoff Rate	Net Increase in Impervious (Proposed - Existing) Flow Rate	Required Reduction of Net Increase in Impervious	Allowable Runoff Rate	Proposed Runoff Rate	
2 Year	0.540 CFS	0.372 CFS	50%	0.354 CFS	0.279 CFS	
10 Year	0.848 CFS	0.585 CFS	25%	0.701 CFS	0.438 CFS	

#### VII. <u>CONCLUSION</u>

The proposed development has been designed with provisions for the safe and efficient control of stormwater runoff in a manner that will not adversely impact the existing drainage patterns, adjacent roadways, or adjacent parcels.

The stormwater management design shall reduce peak flow rates for the proposed development; therefore this project meets the minimum peak flow reduction for the 2 and the 10 year storm frequencies as required by the Standards for Soils Erosion and Sediment Control in New Jersey.



### RUNOFF CURVE NUMBER (CN) CALCULATIONS - EXISTING



#### Existing Drainage Area Summary and Average Curve Number (CN) Calculations

Project: Proposed Multi-Family Residential

Job #: 3639-99-001

Location: Borough of Point Pleasant

Computed By: JM Checked By: KK

Date: Dec. 2020

	Drainage Area	Impervious Area (acre)	Impervious Area (sf)	Curve Number (CN) Used	HSG A - Open Space Area (acre)	HSG A - Open Space Area (sf)	Curve Number (CN) Used	Total Area (acres)	TC (Min.)
	Ex. SA South	0.29	12,693	98	0.45	19,607	39	0.74	13.3
-	Total	0.29	12.693	_	0.45	19.607	- ·	0.74	

Per NR	CS Web Soil Survey -	EveB	HSG	Α	Soil	Evesboro sand, 0 to 5 percent slopes

Description	Runoff Curve Number (CN)
Impervious Surface	98
Open Space (lawn) (good)	39

### RUNOFF CURVE NUMBER (CN) CALCULATIONS -PROPOSED



#### Proposed Drainage Area Summary and Average Curve Number(CN) Calculations

Project: Proposed Multi-Family Residential

Job #: 3639-99-001

Location: Borough of Point Pleasant

Computed By: JM Checked By: KK Date: Dec. 2020

Drainage Area	Impervious Area (acre)	Impervious Area (sf)	Curve Number (CN) Used	HSG A - Open Space Area (acre)	HSG A - Open Space Area (sf)	Curve Number (CN) Used	Total Pervious Area (acres)	Total Area (acres)	TC (Min.)
Prop. SA South	0.15	6,588	98	0.15	6,527	39	0.15	0.30	10.0
Prop. SA Basin A	0.15	6,650	98	0.09	4,040	39	0.09	0.25	10.0
Prop. SA Roof	0.19	8,209	98	0.00	-	39	0.00	0.19	10.0

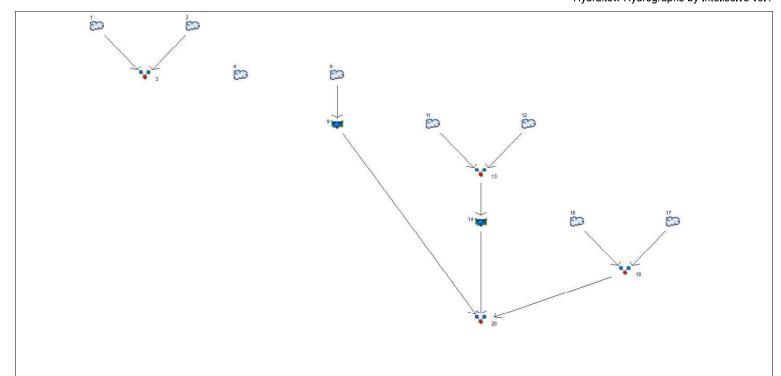
Total 0.49 0.24 0.24 0.73

Per NRCS Web Soil Survey -	EveB	HSG	A	Soil	Evesboro sand, 0 to 5 percent slopes
	_		-		-

Description	Runoff Curve Number (CN)
Impervious Surface	98
Open Space (lawn) (good)	39

#### HYDROGRAPH SUMMARY REPORTS EXISTING AND PROPOSED CONDITIONS 2YR & 10YR STORMS

#### **Watershed Model Schematic**



#### <u>Legend</u>

<u>Hyd.</u>	<u>Origin</u>	<u>Description</u>
1	SCS Runoff	Ex SA South (Imp)
2	SCS Runoff	Ex SA South (Perv)
3	Combine	Ex SA South Total
6	SCS Runoff	Prop Inc in Imp
8	SCS Runoff	Prop SA Roof Total
9	Reservoir	Route to Roof Basin
11	SCS Runoff	Prop SA Basin A (Imp)
12	SCS Runoff	Prop SA Basin A (Perv)
13	Combine	Prop SA Basin A Total
14	Reservoir	Route to Basin A
16	SCS Runoff	Prop SA South (Imp)
17	SCS Runoff	Prop SA South (Perv)
18	Combine	Prop SA South Total
20	Combine	Prop total

Project: 2, 10 yr.gpw

Thursday, Dec 17, 2020

Hydraflow Hydrographs by Intelisolve v9.1

Thursday, Dec 17, 2020

Hydrograph Return Period Recap	•
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2 - Year	
Summary Report	3
Hydrograph Reports	
Hydrograph No. 1, SCS Runoff, Ex SA South (Imp)	4
Hydrograph No. 2, SCS Runoff, Ex SA South (Perv)	
Hydrograph No. 3, Combine, Ex SA South Total	
Hydrograph No. 6, SCS Runoff, Prop Inc in Imp	
Hydrograph No. 8, SCS Runoff, Prop SA Roof Total	
Hydrograph No. 9, Reservoir, Route to Roof Basin	
Pond Report - UG Roof Basin	
Hydrograph No. 11, SCS Runoff, Prop SA Basin A (Imp)	
Hydrograph No. 12, SCS Runoff, Prop SA Basin A (Perv)	
Hydrograph No. 13, Combine, Prop SA Basin A Total	
Hydrograph No. 14, Reservoir, Route to Basin A	
Pond Report - AG Basin A	
Hydrograph No. 16, SCS Runoff, Prop SA South (Imp)	
Hydrograph No. 17, SCS Runoff, Prop SA South (Perv)	
Hydrograph No. 18, Combine, Prop SA South Total	
Hydrograph No. 20, Combine, Prop total	
10 - Year	
Summary Report	20
Hydrograph Reports	
Hydrograph No. 1, SCS Runoff, Ex SA South (Imp)	
Hydrograph No. 2, SCS Runoff, Ex SA South (Perv)	
Hydrograph No. 3, Combine, Ex SA South Total	23
Hydrograph No. 6, SCS Runoff, Prop Inc in Imp	
Hydrograph No. 8, SCS Runoff, Prop SA Roof Total	
Hydrograph No. 9, Reservoir, Route to Roof Basin	
Hydrograph No. 11, SCS Runoff, Prop SA Basin A (Imp)	
Hydrograph No. 12, SCS Runoff, Prop SA Basin A (Perv)	
Hydrograph No. 13, Combine, Prop SA Basin A Total	
Hydrograph No. 14, Reservoir, Route to Basin A	
Hydrograph No. 16, SCS Runoff, Prop SA South (Imp)	
Hydrograph No. 17, SCS Runoff, Prop SA South (Perv)	
Hydrograph No. 18, Combine, Prop SA South Total	
Hydrograph No. 20, Combine, Prop total	
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IDF Report	35

# Hydrograph Summary Report

Hydraflow Hydrographs by Intelisolve v9.1

No.	1	7	က	9	œ	თ	F	12	13	4	16	17	8	70	Proj
Hydrograph description	Ex SA South (Imp)	Ex SA South (Perv)	Ex SA South Total	Prop Inc in Imp	Prop SA Roof Total	Route to Roof Basin	Prop SA Basin A (Imp)	Prop SA Basin A (Perv)	Prop SA Basin A Total	Route to Basin A	Prop SA South (Imp)	Prop SA South (Perv)	Prop SA South Total	Prop total	Thursday, Dec 17, 2020
Total strge used (cuft)						2,184				1,726	1	}	ļ		Thursday, [
Maximum elevation (ft)		-				11.67		}	-	13.49		}			ar
Inflow hyd(s)	-		1, 2			œ	-	1	11, 12	13	-	}	16, 17	9, 14, 18,	Retum Period: 2 Year
Hyd. volume (cuft)	3,333	6	3,342	2,299	2,184	0	1,724	2	1,726	0	1,724	ဂ	1,727	1,727	Return P
Time to peak (min)	730	1430	730	730	730	n/a	730	1430	730	n/a	730	1430	730	730	
Time interval (min)	2	5	2	2	2	2	5	2	2	S	2	2	2	2	
Peak flow (cfs)	0.540	0.001	0.540	0.372	0.354	0.000	0.279	0.000	0.279	0.000	0.279	0.000	0.279	0,279	
Hydrograph type (origin)	SCS Runoff	SCS Runoff	Combine	SCS Runoff	SCS Runoff	Reservoir	SCS Runoff	SCS Runoff	Combine	Reservoir	SCS Runoff	SCS Runoff	Combine	Combine	2, 10 yr.gpw
No.	-	7	က	9	œ	6	F	12	13	4	16	17	81	20	2, 1

# Hydrograph Return Period Recap

Hydraflow Hydrographs by Intelisolve v9.1

-											
ž ž	£	Hyd(s)				reak out	reak Outllow (cis)				description
	(origin)		1 <del>.</del> Yr	2-Yr	3-Yr	5-Yr	10-Yr	25-Yr	50-Yr	100-Yr	
-	SCS Runoff	-		0.540	-		0.848	İ			Ex SA South (Imp)
2	SCS Runoff		-	0.001	1	I	0.022	İ	-	ļ	Ex SA South (Perv)
ო	Combine	1,2	İ	0.540	-		0.848				Ex SA South Total
9	SCS Runoff			0.372			0.585				Prop Inc in Imp
80	SCS Runoff	ļ		0.354			0.555				Prop SA Roof Total
თ	Reservoir	∞		0.000	-		0.000				Route to Roof Basin
£	SCS Runoff			0.279	-		0.438				Prop SA Basin A (Imp)
12	SCS Runoff	İ		0.000	ł		0.004	İ			Prop SA Basin A (Perv)
13	Combine	11, 12		0.279			0.438				Prop SA Basin A Total
4	Reservoir	13		0.000			0.159				Route to Basin A
16	SCS Runoff	İ		0.279			0.438				Prop SA South (Imp)
17	SCS Runoff	ļ	ļ	0.000	1		2000		ļ	ļ	Prop SA South (Perv)
. 60	Combine	16. 17	ļ	0.279	ļ		0.438	1	1	ļ	Prop SA South Total
2		: 2		2							
20	Combine	9, 14, 18,		0.279	1		0.438				Prop total
Pro	Proj. file: 2, 10 yr.gpw	wdb.							     H	ırsday, E	Thursday, Dec 17, 2020

Hyd. No. 2

Hydraflow Hydrographs by Intelisolve v9.1

Ex SA South (Perv)

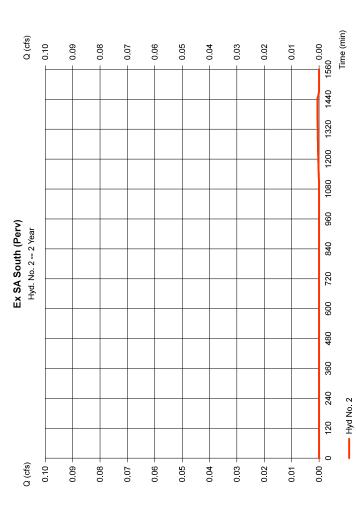
Peak discharge = 0.001 cfs
Time to peak = 1430 min
Hyd. volume = 9 cuft
Curve number = 39
Hydraulic length = 0 ft
Time of conc. (Tc) = 13.30 min
Distribution = Custom
Shape factor = 285 = SCS Runoff = 2 yrs = 0.450 ac = 0.05% = USER = 3.42 in = NOAAAtlas 14 Type-D.cds Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration

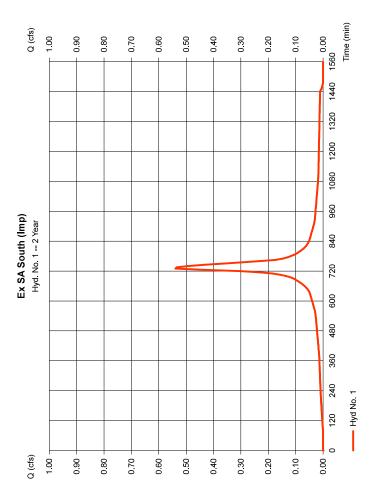
2

Thursday, Dec 17, 2020

**Hydrograph Report** 

Thursday, Dec 17, 2020 = 0.540 cfs = 730 min = 3,333 cuft = 98 = 0 ft = 10.00 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor Peak discharge Time to peak Hyd. volume = SCS Runoff = 2 yrs = 5 min = 0.290 ac = 0.0 % = USER = 3.42 in = NOAA Atlas 14 Type-D.cds Hydraflow Hydrographs by Intelisolve v9.1 Ex SA South (Imp) Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration Hyd. No. 1





Hyd. No. 6

Hydraflow Hydrographs by Intelisolve v9.1

Prop Inc in Imp

= SCS Runoff = 2 yrs = 5 min = 0.200 ac = 0.00 % = USER = 3.42 in = NOAA Atlas 14 Type-D.cds Hydrograph type Storm frequency Time interval

Drainage area Basin Slope Tc method Total precip. Storm duration

Thursday, Dec 17, 2020 = 0.372 cfs = 730 min = 2,299 cuft = 98 = 0 ft = 10.00 min = Custom = 285 Peak discharge
Time to peak
Hyd. volume
Curve number
Hydraulic length
Time of conc. (TC)
Distribution
Shape factor

# **Hydrograph Report**

Hydraflow Hydrographs by Intelisolve v9.1

Thursday, Dec 17, 2020

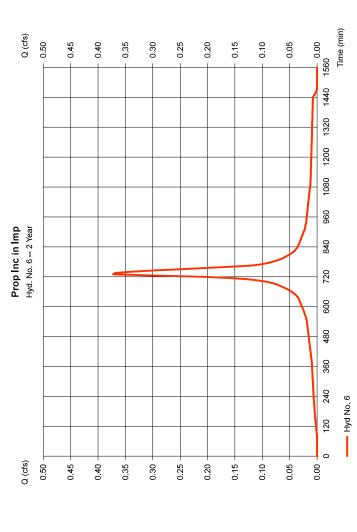
9

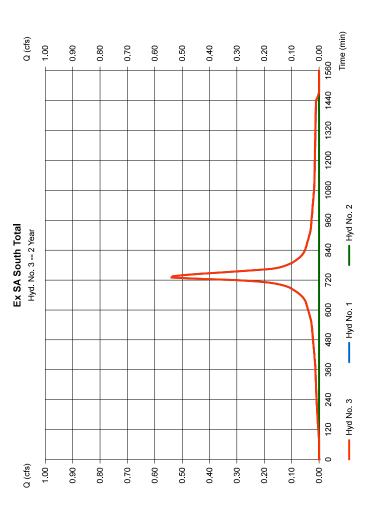
Hyd. No. 3

Ex SA South Total

= Combine = 2 yrs = 5 min = 1, 2 Hydrograph type Storm frequency Time interval Inflow hyds.

Peak discharge = 0.540 cfs
Time to peak = 730 min
Hyd. volume = 3,342 cuft
Contrib. drain. area = 0.740 ac





Hydraflow Hydrographs by Intelisolve v9.1

Hyd. No. 9

Route to Roof Basin

= 0.000 cfs = n/a = 0 cuft = 11.67 ft = 2,184 cuft Peak discharge Time to peak Hyd. volume Max. Elevation Max. Storage Reservoir2 yrs5 min8 - Prop SA Roof TotalUG Roof Basin Hydrograph type Storm frequency Time interval Inflow hyd. No.

Reservoir name

Storage Indication method used.

6

Thursday, Dec 17, 2020

**Hydrograph Report** 

Thursday, Dec 17, 2020 Hydraflow Hydrographs by Intelisolve v9.1

Hyd. No. 8

Prop SA Roof Total

Hydrograph type Storm frequency Time interval

Peak discharge Time to peak Hyd. volume

Drainage area Basin Slope Tc method Total precip. Storm duration

Q (cfs)

Route to Roof Basin Hyd. No. 9 -- 2 Year

> Q (cfs) 0.50

0.45

0.40

0.35

0.30

0.20

0.15

0.25

0.10

0.05

0.50

0.45

0.40

0.35

0.30

0.25

0.20

0.15

0.10

0.05

= SCS Runoff = 2 yrs = 5 min = 0.190 ac = 0.0 % = USER = 3.42 in = NOAA Atlas 14 Type-D.cds

= 0.354 cfs = 730 min = 2,184 cuft = 98 = 0 ft = 10.00 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor

Time (min) Q (cfs) 0.15 0.10 0.00 0.50 0.45 0.40 0.20 0.05 0.35 0.30 0.25 1560 1440 1320 1200 1080 960 Prop SA Roof Total Hyd. No. 8 -- 2 Year 840 720 900 480 360 240 120 0 Q (cfs) 0.50 0.10 0.45 0.40 0.35 0.30 0.20 0.15 0.00 0.25 0.05

—— Hyd No. 8

Time (min)

0.00

1560 1440

1320

1200

1080

960

840

720

900

480

360

240

120

0

0.00

Total storage used = 2,184 cuft

—— Hyd No. 8

Hyd No. 9

## Hyd. No. 11

Hydraflow Hydrographs by Intelisolve v9.1

Prop SA Basin A (Imp)

= SCS Runoff = 2 yrs = 5 min = 0.150 ac = 0.0 % = USER = 3.42 in = NOAA Atlas 14 Type-D.cds Hydrograph type Storm frequency Time interval

Drainage area Basin Slope Tc method Total precip. Storm duration

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Thursday, Dec 17, 2020

Peak discharge = 0.279 cfs
Time to peak = 730 min
Hyd. volume = 1,724 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 10.00 min
Distribution = Custom
Shape factor = 285

Time (min) Q (cfs) 0.00 0.10 0.50 0.45 0.40 0.35 0.30 0.25 0.20 0.15 0.05 1440 1560 1320 1080 1200 960 Prop SA Basin A (Imp) Hyd. No. 11 – 2 Year 840 720 900 480 360 240 120 0 Q (cfs) 0.50 0.40 0.10 00.00 0.45 0.35 0.30 0.20 0.15 0.25 0.05

—— Hyd No. 11

**Pond Report** 

Thursday, Dec 17, 2020

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Pond No. 2 - UG Roof Basin

Hydraflow Hydrographs by Intelisolve v9.1

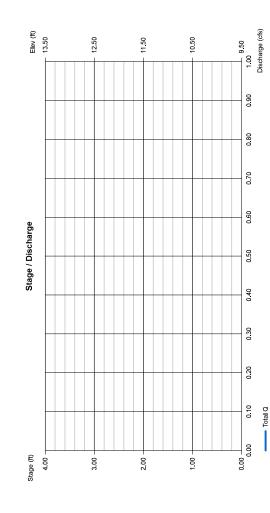
Pond Data

UG Chambers - Invert elev. = 10.00 ft, Rise x Span = 2.00 x 2.00 ft, Barrel Len = 65.00 ft, No. Barrels = 4, Slope = 0.00%, Headers = Yes Encasement - Invert elev. = 9.50 ft, Width = 3.50 ft, Height = 3.50 ft, Voids = 100.00%

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orage T
ge / Sto
Sta

Flevation (ff)   Contour area (sqft)	Stage / Storage Table	age Table							
10.20   10.2	Stage (ft)	Elevation (ft)	Contour	area (sqft)	Incr. Storage (cuft)	Total storag	e (cuft)		
10.55   10.4   3.55	0.00	9.50	_	/a	0	0	_		
10.20	0.35	9.85	_	/a	353	353			
10.55   n/a   353   1.059	0.70	10.20	_	/a	353	902			
10.90	1.05	10.55	_	/a	353	1,059			
1125   n/a   353   1,764     1166   n/a   353   2,470     1130   n/a   353   2,470     1230   n/a   353   2,470     1230   n/a   353   2,470     1230   n/a   353   2,470     13,00   n/a   353   3,176     13,00   0.00   0.00   0.00   0.00     14,00   0.00   0.00   0.00   0.00     15,00   0.00   0.00   0.00     15,00   0.00	1.40	10.90	_	/a	353	1,411			
1150	1.75	11.25	_	/a	353	1,764			
11,95   11,97   11,97   11,97   11,97   11,97   11,97   11,97   11,2	2.10	11.60	_	/a	353	2,117			
12.50   n/a   353   2.823   17.50   n/a   35.50   3.529   17.50   n/a   35.50   3.529   3.529   17.50   n/a   3.529	2.45	11.95	_	/a	353	2,470			
12.65   12.65   10.6   353   3.176	2.80	12.30	_	/a	353	2,823			
13.00   n/a   353   3,529     Orifice Structures	3,15	12.65		la/	353	3.176			
Orifice Structures	3.50	13.00	_	l/a	353	3,529			
	Culvert / Ori	ifice Structures			Weir Structure	S			
100   100		₹		_		₹	<u>@</u>	<u>ত</u>	<u> </u>
s         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         0.00         Weif Type         =  <	Rise (in)	0.00			Crest Len (ft)	= 0.00	0.00	0.00	0.00
s         =         0         0         0         Weir Coeff.         =         3.33	Span (in)	00.00			Crest El. (ft)	= 0.00	0.00	0.00	0.00
tt)         = 0.00         0.00         0.00         0.00         Weir Type         =   <	No. Barrels	0			Weir Coeff.		3.33	3.33	3.33
= 0.00	Invert El. (ft)	00.00			Weir Type		i	1	1
= 0.00 0.00 0.00 n/a = 0.13 0.13 n/a n/a eff. = 0.60 0.60 0.60 ExfL(m/nr) e = n/a No No No TVV Elev.(tt)	Length (ft)	0.00			Multi-Stage		٩	٩	No
= .013 .013 n/a eff. = 0.60 0.60 0.60 Exfil.(in/hr) e = n/a No No TW Elev. (ft)	Slope (%)	00.00							
= 0.60 0.60 0.60 Exfil.(in/hr) = n/a No No No TW Elev. (ft)	N-Value	013							
= n/a No No TW Elev. (ft) =	Orifice Coeff.	09'0			Exfil.(in/hr)	= 0.000 (by W	et area)		
	Multi-Stage				TW Elev. (ft)	= 0.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (oc) control. Weir risers checked for orifice conditions (ic) and submergence (s).



Hydraflow Hydrographs by Intelisolve v9.1

## Hyd. No. 13

Prop SA Basin A Total

= Combine = 2 yrs = 5 min = 11, 12 Hydrograph type Storm frequency Time interval

Inflow hyds.

Peak discharge = 0.279 cfs
Time to peak = 730 min
Hyd. volume = 1,726 cuft
Contrib. drain. area = 0.240 ac

# Hydrograph Report

Thursday, Dec 17, 2020 Hydraflow Hydrographs by Intelisolve v9.1

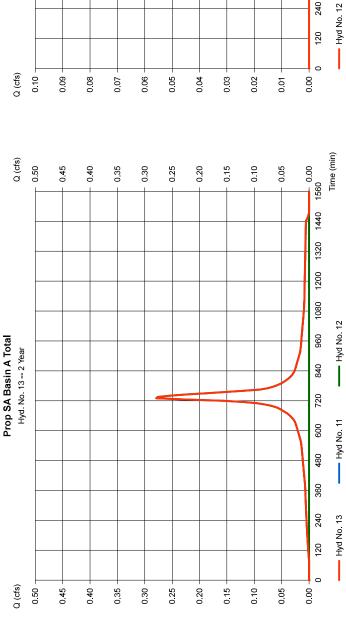
## Hyd. No. 12

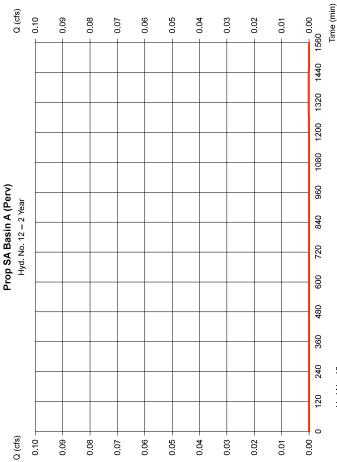
Thursday, Dec 17, 2020

5

Prop SA Basin A (Perv)

= 0.000 cfs = 1430 min = 2 cuft = 39 = 0 ft = 10.00 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor Peak discharge Time to peak Hyd. volume = SCS Runoff = 2 yrs = 5 min = 0.090 ac = 0.0 % = USER = 3.42 in = NOAA Atlas 14 Type-D.cds Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration





# Pond Report

Hydraflow Hydrographs by Intelisolve v9.1 Thursday, Dec 17, 2020 Pond No. 1 - AG Basin A

Pond Data

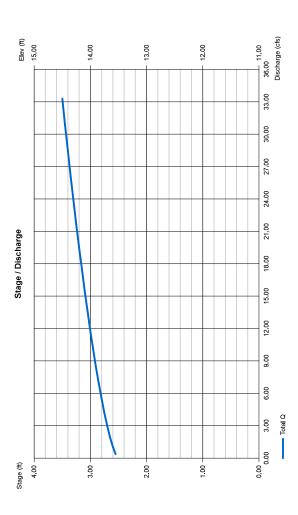
Stage / Storage Table

Contours - User-defined contour areas. Conic method used for volume calculation. Begining Elevation = 11.00 ft

	Total storage (cuft)	0	377	1,165	1,742	2,448	3,237
	Incr. Storage (cuft)	0	377	788	578	202	788
	Contour area (sqft)	220	260	1,040	1,275	1,554	1,600
age lable	Elevation (ft)	11.00	12.00	13.00	13.50	14.00	14.50
Stage / Stotage Table	Stage (ft)	0.00	1.00	2.00	2.50	3.00	3.50

Culvert / Ori	Sulvert / Orifice Structures	s			Weir Structures	res			
	Ā	<u>@</u>	<u>ত</u>	[PrfRsr]		₹	<u>@</u>	<u>ত</u>	<u> </u>
Rise (in)	00.0 =	0.00	0.00	00.00	Crest Len (ft)	= 10.00	00.00	00.00	00.00
Span (in)	= 0.00	0.00	0.00	00.00	Crest El. (ft)	= 13.50	0.00	0.00	0.00
No. Barrels	0 =	0	0	0	Weir Coeff.	= 3.33	3.33	3.33	3.33
Invert El. (ft)	= 0.00	0.00	0.00	00.00	Weir Type	= Rect	1	1	1
Length (ft)	00'0 =	0.00	0.00	00.00	Multi-Stage	oN =	õ	8 N	٩
Slope (%)	= 0.00	0.00	0.00	n/a					
N-Value	= .013	.013	.013	n/a					
Orifice Coeff.	09'0 =	09.0	09.0	09.0	Exfil (in/hr)	(q) 000 0 =	0.000 (by Wet area)		
Multi-Stage	= n/a	8	8	% N	TW Elev. (ft)	00.00			

Note: Culvert/Orifice outflows are analyzed under inlet (ic) and outlet (ac) control. Weir risers checked for orifice conditions (ic) and submergence (s).



# Hydrograph Report

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Hydraflow Hydrographs by Intelisolve v9.1 Thursday, Dec 17, 2020

4

## Hyd No 14

Route to Basin A

Hydrograph type = Reservoir

Storm frequency = 2 yrs

Time to peak = n/a

Time to peak = n/a

Time to peak = n/a

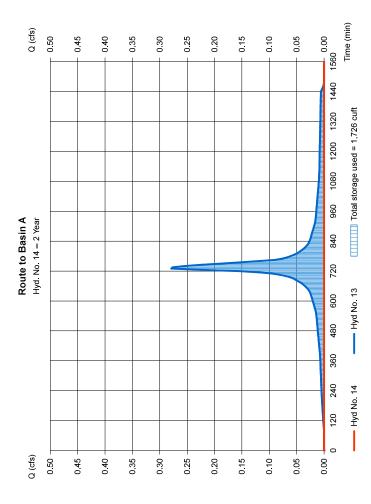
Time to peak = n/a

Hyd. volume = 0 cuft

Inflow hyd. No. = 13 - Prop SA Basin A Total Max. Elevation = 13.49 ft

Reservoir name = AG Basin A Max. Storage = 1,726 cuft

Storage Indication method used.



Hydraffow Hydrographs by Intelisolve v9.1

## Hyd. No. 17

Prop SA South (Perv)

Hydrograph typeSCS RunoffPeak discharge= 0.000 cfsStorm frequency= 2 yrsTime to peak= 1430 minTime interval= 5 minHyd. volume= 3 cuftDrainage area= 0.150 acCurve number= 39Basin Slope= 0.0 %Hydraulic length= 0 ftTo method= USERTime of conc. (To)= 10.00 minTotal precip.= 3.42 inDistribution= CustomStorm duration= NOAAAAtlas 14 Type-D.cdsShape factor= 285

# Hydrograph Report

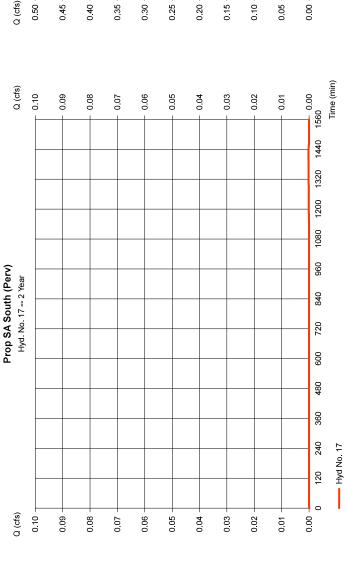
1

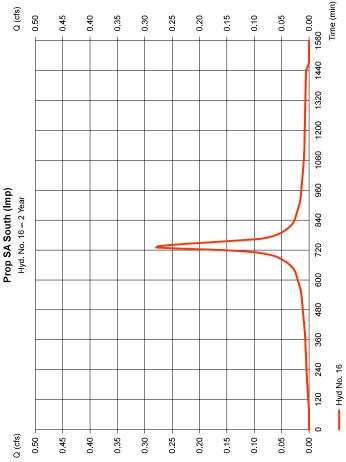
Hydraflow Hydrographs by Intelsolve v9.1 Thursday, Dec 17, 2020

## Hyd No 16

Thursday, Dec 17, 2020

Prop SA South (Imp)





Thursday, Dec 17, 2020

## 19

Hydraflow Hydrographs by Intelisolve v9.1

**Hydrograph Report** 

Hyd. No. 20

Prop total

= Combine = 2 yrs = 5 min = 9, 14, 18 Hydrograph type Storm frequency Time interval Inflow hyds.

Peak discharge = 0.279 cfs
Time to peak = 730 min
Hyd. volume = 1,727 cuft
Contrib. drain. area = 0.000 ac

**Hydrograph Report** 

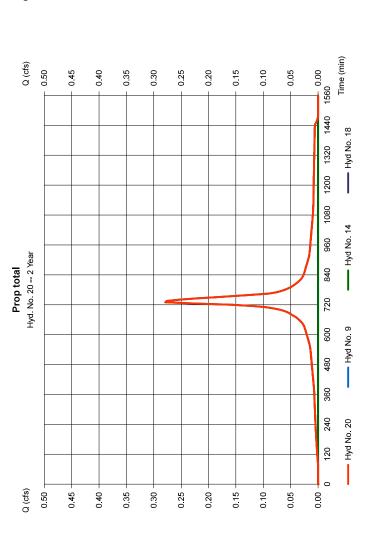
Hydraflow Hydrographs by Intelisolve v9.1

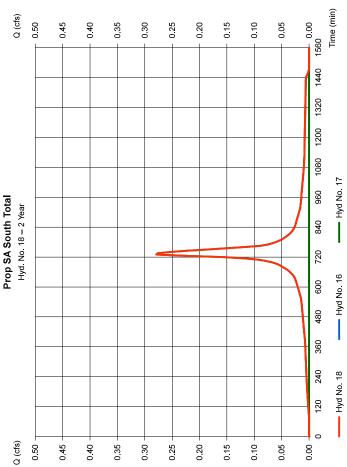
Thursday, Dec 17, 2020

Prop SA South Total

Hyd No 18

Peak discharge = 0.279 cfs
Time to peak = 730 min
Hyd. volume = 1,727 cuft
Contrib. drain. area = 0.300 ac = Combine = 2 yrs = 5 min = 16, 17 Hydrograph type Storm frequency Time interval Inflow hyds.





Hydraflow Hydrographs by Intelisolve v9.1

Thursday, Dec 17, 2020

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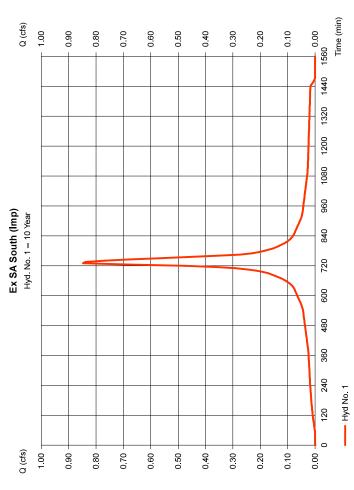
Hyd. No. 1

Ex SA South (Imp)

= SCS Runoff = 10 yrs = 5 min = 0.290 ac = 0.0 % = USER = 5.33 in = NOAA Atlas 14 Type-D.cds

Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip.

Peak discharge = 0.848 cfs
Time to peak = 730 min
Hyd. volume = 5,327 cuft
Curve number = 98
Hydraulic length = 0 ft
Time of conc. (Tc) = 10.00 min
Distribution = Custom
Shape factor = 285



# **Hydrograph Summary Report**

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Hyd. No.	Hydrograph type (origin)	Peak flow (cfs)	Time interval (min)	Time to peak (min)	Hyd. volume (cuft)	Inflow hyd(s)	Maximum elevation (ft)	Total strge used (cuft)	Hydrograph description
-	SCS Runoff	0.848	2	730	5,327	!		-	Ex SA South (Imp)
2	SCS Runoff	0.022	2	775	440	I		ļ	Ex SA South (Perv)
ო	Combine	0.848	2	730	5,767	1, 2		-	Ex SA South Total
9	SCS Runoff	0,585	22	730	3,674			1	Prop Inc in Imp
80	SCS Runoff	0.555	2	730	3,490	ļ	l	-	Prop SA Roof Total
6	Reservoir	0.000	2	n/a	0	ø.	12.96	3,490	Route to Roof Basin
7	SCS Runoff	0.438	2	730	2,755	ļ			Prop SA Basin A (Imp)
12	SCS Runoff	0.004	s	775	88	ļ		-	Prop SA Basin A (Perv)
13	Combine	0.438	c2	730	2,843	11, 12	İ	-	Prop SA Basin A Total
4	Reservoir	0.159	22	765	1,101	13	13.52	1,773	Route to Basin A
16	SCS Runoff	0.438	2	730	2,755	ļ	į	}	Prop SA South (Imp)
17	SCS Runoff	0.007	2	775	147	1		}	Prop SA South (Perv)
92	Combine	0.438	25	730	2,902	16, 17		}	Prop SA South Total
20	Combine	0.438	ro	730	4,003	9, 14, 18,		}	Prop total
2, 1	2, 10 yr.gpw				Return P	Return Period: 10 Year	ear	Thursday, D	Thursday, Dec 17, 2020

Hydraflow Hydrographs by Intelisolve v9.1

## Hyd. No. 3

Ex SA South Total

= Combine = 10 yrs = 5 min = 1, 2 Hydrograph type Storm frequency Time interval

Inflow hyds.

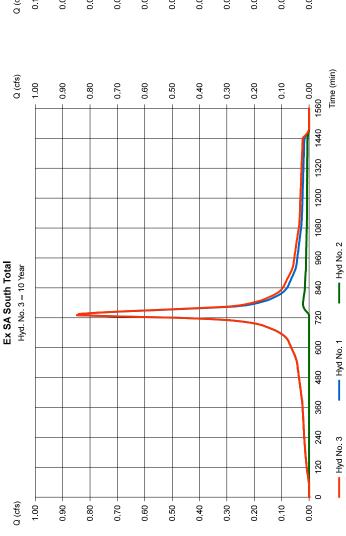
Thursday, Dec 17, 2020

Peak discharge = 0.848 cfs
Time to peak = 730 min
Hyd. volume = 5,767 cuft
Contrib. drain. area = 0.740 ac

# Hydrograph Report

23

Thursday, Dec 17, 2020 = 0.022 cfs = 775 min = 440 cuft = 39 = 0 ft = 13.30 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor Peak discharge Time to peak Hyd. volume = SCS Runoff = 10 yrs = 5 min = 0.450 ac = 0.0 % = USER = 5.33 in = NOAA Atlas 14 Type-D.cds Hydraflow Hydrographs by Intelisolve v9.1 Ex SA South (Perv) Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration Hyd. No. 2





Hydraflow Hydrographs by Intelisolve v9.1

### Hyd. No. 8

Prop SA Roof Total

Hydrograph type = SCS Runoff Storm frequency = 10 yrs

Time interval = 5 min Hyd. volume Drainage area = 0.190 ac Curve numb Brain Slope = 0.0 % Hydralic leasures of the control of the c

Thursday, Dec 17, 2020

25

Peak discharge = 0.555 cfs
Time to peak = 730 min
Hyd. volume = 3.490 cuft
Curve number = 98
Hydraulic length = 0.ft
Time of conc. (Tc) = 10.00 min
Distribution = Custom
Shape factor = 285

# Hydrograph Report

 Hydr. No. 6
 Thursday, Dec 17, 2020

 Prop Inc in Imp
 Prop Inc in Imp
 Peak discharge
 = 0.585 cfs

 Hydrograph type
 = SCS Runoff
 Peak discharge
 = 0.585 cfs

 Storm frequency
 = 10 yrs
 Time to peak
 = 730 min

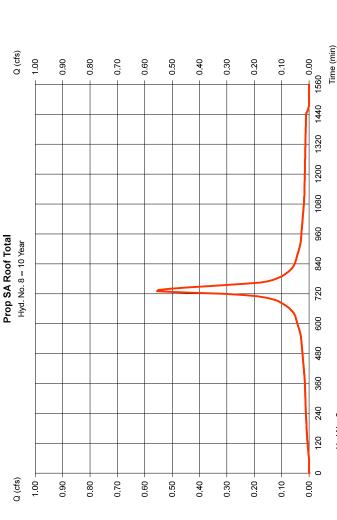
 Time interval
 = 5 min
 Hydr volume
 = 3.674 cuft

 Drainage area
 = 0.00 %
 Hydraulic length
 = 0.6

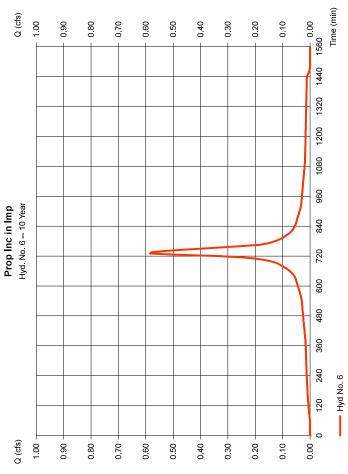
 Basin Slope
 = 0.0 %
 Hydraulic length
 = 0 ft

 Total precip.
 = 5.33 in
 Distribution
 = Custom

 Storm duration
 = NOAAAtlas 14 Type-D.cds
 Shape factor
 = 285



Hyd No. 8



Hydraflow Hydrographs by Intelisolve v9.1

Hyd. No. 11

Prop SA Basin A (Imp)

= 0.438 cfs = 730 min = 2,755 cuft = 98 = 0 ft = 10.00 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor Peak discharge Time to peak Hyd. volume = SCS Runoff = 10 yrs = 5 min = 0.150 ac = 0.0 % = USER = 5.33 in = NOAAAtlas 14 Type-D.cds Hydrograph type Drainage area Basin Slope Tc method Total precip. Storm duration Storm frequency Time interval

27

Thursday, Dec 17, 2020

**Hydrograph Report** 

Thursday, Dec 17, 2020 Hydraflow Hydrographs by Intelisolve v9.1

Hyd No. 9

Route to Roof Basin

Storm frequency Time interval Inflow hyd. No. Hydrograph type

Reservoir name

Reservoir10 yrs5 min8 - Prop SA Roof TotalUG Roof Basin

= n/a = 0 cuft = 12.96 ft = 3,490 cuft

Peak discharge Time to peak Hyd. volume Max. Elevation Max. Storage

= 0.000 cfs

Storage Indication method used.

Route to Roof Basin Hyd. No. 9 -- 10 Year

0.90

0.45

0.80

0.40

0.70

0.35

0.60

0.30

0.50

0.25

Q (cfs)

Q (cfs) 90.

Q (cfs)

Prop SA Basin A (Imp) Hyd. No. 11 -- 10 Year

Q (cfs)

0.50

0.45

0.40

0.35

0.30

0.20

0.15

0.25

0.10

0.05

0.50

1.00 0.90

0.80

0.70

0.60

0.40

0.20

0.20

0.10 0.05

0.10

0.30

0.15

0.40

0.50

0.30

0.20

900 480

360

240

120

0

0.00

0.00

1560

1440

1320

1080 1200

960

840

720

900

480

360

240

120

0

0.00

—— Hyd No. 11

720

840

Total storage used = 3,490 cuft

--- Hyd No. 8

—— Hyd No. 9

Time (min)

1320

Time (min)

0.00

1560

1440

0.10

1200 1080

960

Hydraflow Hydrographs by Intelisolve v9.1

Hyd. No. 13

Prop SA Basin A Total

= Combine = 10 yrs = 5 min = 11, 12 Hydrograph type Storm frequency Time interval

Inflow hyds.

Peak discharge = 0.438 cfs
Time to peak = 730 min
Hyd. volume = 2,843 cuft
Contrib. drain. area = 0.240 ac

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Hydrograph Report

Thursday, Dec 17, 2020

Hyd. No. 12

Hydraflow Hydrographs by Intelisolve v9.1

Thursday, Dec 17, 2020

Prop SA Basin A (Perv)

Hydrograph type Storm frequency Time interval

Peak discharge Time to peak Hyd. volume

Drainage area Basin Slope Tc method Total precip. Storm duration

Q (cfs)

Prop SA Basin A Total Hyd. No. 13 -- 10 Year

> Q (cfs) 0.50

0.45

0.40

0.35

0.30

0.20

0.15

0.25

0.10

0.05

0.50

0.45

0.40

0.35

0.30

0.25

0.20

0.15

= SCS Runoff = 10 yrs = 5 min = 0.090 ac = 0.0 % = USER = 5.33 in = NOAA Atlas 14 Type-D.cds

= 0.004 cfs = 775 min = 88 cuft = 39 = 0 ft = 10.00 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor

Q (cfs) 0.10 0.09 0.08 0.07 0.06 0.05 0.04 0.03 Prop SA Basin A (Perv) Hyd. No. 12 -- 10 Year Q (cfs) 0.10 0.09 0.08 90.0 0.04 0.07 0.05 0.03

120 0

Time (min)

—— Hyd No. 12

Time (min)

0.00

1560

1440

1320

1200

1080

960

840

720

900

480

360

240

0.00

0.00

1560

1440

1320

1200

1080

840

720

900

480

360

240

120

0

00.0

—— Hyd No. 12 960

--- Hyd No. 11

--- Hyd No. 13

0.02

0.10

0.01

0.05

0.02

0.01

8

## **Hydrograph Report**

Hydraflow Hydrographs by Intelsolve v9.1

## Hyd. No. 16

Prop SA South (Imp)

Hydrograph typeSCS RunoffPeak discharge= 0.438 cfsStorm frequency= 10 yrsTime to peak= 730 minTime interval= 5 minHyd. volume= 2,755 cuftDrainage area= 0.150 acHydraulic length= 0 ftBasin Slope= 0.0 %Hydraulic length= 0 ftTo method= USERTime of conc. (Tc)= 10.00 minTotal precip.= 5.33 inDistribution= CustomStorm duration= NOAA Atlas 14 Type-D.cdsShape factor= 285

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Thursday, Dec 17, 2020

**Hydrograph Report** 

Hydrographs by Intelsolve v9.1 Thursday, Dec 17, 2020

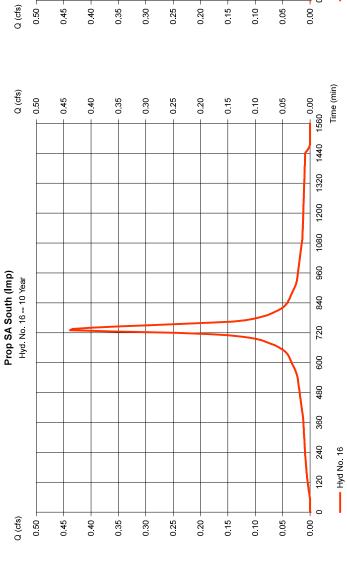
## Hyd. No. 14

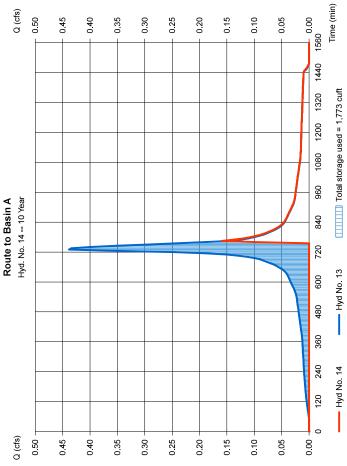
Route to Basin A

Hydrograph type = Reservoir
Storm frequency = 10 yrs
Time interval = 5 min
Inflow hyd. No. = 13 - Prop SA Basin A Total
Reservoir name = AG Basin A

Peak discharge = 0.159 cfs
Time to peak = 765 min
Hyd. volume = 1,101 cuft
Max. Elevation = 13.52 ft
Reservoir name = AG Basin A

Storage Indication method used.





Hydraflow Hydrographs by Intelisolve v9.1

## Hyd. No. 18

Prop SA South Total

= Combine = 10 yrs = 5 min = 16, 17 Hydrograph type Storm frequency Time interval

Peak discharge = 0.438 cfs
Time to peak = 730 min
Hyd. volume = 2,902 cuft
Contrib. drain. area = 0.300 ac

Inflow hyds.

# Hydrograph Report

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Thursday, Dec 17, 2020

Thursday, Dec 17, 2020 Hydraflow Hydrographs by Intelisolve v9.1

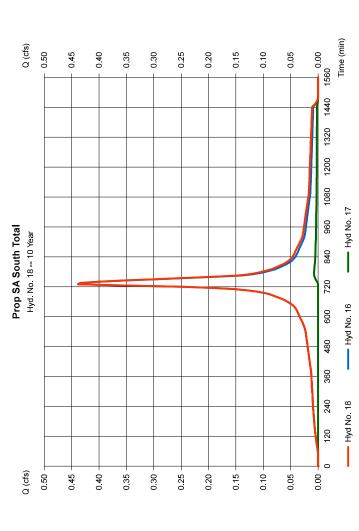
## Hyd. No. 17

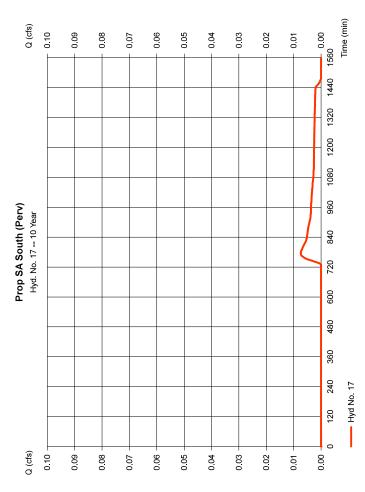
Prop SA South (Perv)

= SCS Runoff = 10 yrs = 5 min = 0.150 ac = 0.0 % = USER = 5.33 in = NOAA Atlas 14 Type-D.cds Hydrograph type Storm frequency Time interval Drainage area Basin Slope Tc method Total precip. Storm duration

Peak discharge Time to peak Hyd. volume

= 0.007 cfs = 775 min = 147 cuft = 39 = 0 ft = 10.00 min = Custom = 285 Curve number
Hydraulic length
Time of conc. (Tc)
Distribution
Shape factor





Hydraflow Hydrographs by Intelisolve v9.1

Return	Intensity-	Intensity-Duration-Frequency Equation Coefficients (FHA)	Equation Coefficient	s (FHA)
(Yrs)	В	Q	3	(N/A)
-	39.0824	9.5000	0.8528	
2	45.6943	10.7000	0.8185	
e	0.000	0.000	0.000	
2	99.7061	14.8000	0.9304	
10	249.7597	21.8001	1.0961	1
25	115.7547	14.9000	0.8980	
50	7.3699	0.1000	0.2544	
100	403.8513	25.1001	1.1108	

File name: TRENTON.idf

## Intensity = B / (Tc + D)^E

Return					Intens	Intensity Values (in/hr)	(in/hr)					
(Yrs)	5 min	10	15	20	25	30	35	40	45	90	22	09
1	4.00	3.10	2.55	2.18	1.91	1.70	1.54	1.40	1.29	1.20	1.12	1.05
7	4.80	3.83	3.21	2.77	2.45	2.20	2.00	1.84	1.70	1.59	1.49	1.40
ღ	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00	00.00
2	6.20	5.03	4.24	3.67	3.24	2.90	2,63	2.40	2.22	2.06	1.92	1.80
10	6.80	5,63	4.80	4.17	3.69	3,30	2.98	2.72	2.50	2.31	2.14	2.00
25	7.89	6.45	5.47	4.76	4.23	3.80	3.46	3.17	2.93	2.73	2.55	2.40
20	4.87	4.09	3.69	3.44	3.25	3.10	2.98	2.88	2.80	2.72	2.66	2.60
100	9.20	7.76	69.9	5.87	5.22	4.70	4.27	3.91	3.60	3.33	3.10	2.90

Tc = time in minutes. Values may exceed 60.

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		œ	Rainfall Precipitation Table (in)	recipitat	ion Tab	e (in)		
Storm Distribution	1-yr	2-yr	3-уг	5-yr	10-yr	25-yr	50-yr	100-yr
SCS 24-hour	00'0	3.42	0.00	0.00	5.33	6.68	0.00	9.20
SCS 6-Hr	0.00	0.00	0.00	0.00	0.00	0.00	00.00	0.00
Huff-1st	0.00	00.00	0.00	0.00	0.00	00.00	0.00	00.00
Huff-2nd	00.00	00.00	00.0	00.0	0.00	00.00	0.00	00.00
Huff-3rd	00.00	00.00	00.00	00.0	00.00	0.00	00.00	00.00
Huff-4th	00.00	00.00	00.00	00.00	00'0	00.00	00.00	00.0
Huff-Indy	00.00	00'0	00.00	00.0	00'0	00.00	00.00	00.00
Custom	1.25	3,42	00.00	00.00	5.33	89.9	00.00	9.20

# Hydrograph Report

Hydraflow Hydrographs by Intelisolve v9.1

Thursday, Dec 17, 2020

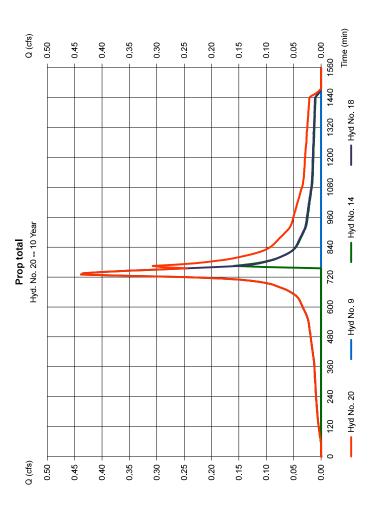
34

Hyd. No. 20

Prop total

= Combine = 10 yrs = 5 min = 9, 14, 18 Hydrograph type Storm frequency Time interval Inflow hyds.

Peak discharge = 0.438 cfs
Time to peak = 730 min
Hyd. volume = 4,003 cuft
Contrib. drain. area = 0.000 ac



### WEB SOIL SURVEY MAP



#### MAP LEGEND MAP INFORMATION The soil surveys that comprise your AOI were mapped at Area of Interest (AOI) С 1:24.000. Area of Interest (AOI) C/D Soils Warning: Soil Map may not be valid at this scale. D Soil Rating Polygons Enlargement of maps beyond the scale of mapping can cause Not rated or not available Α misunderstanding of the detail of mapping and accuracy of soil **Water Features** line placement. The maps do not show the small areas of A/D contrasting soils that could have been shown at a more detailed Streams and Canals Transportation B/D Rails ---Please rely on the bar scale on each map sheet for map measurements. Interstate Highways C/D Source of Map: Natural Resources Conservation Service **US Routes** Web Soil Survey URL: D Major Roads Coordinate System: Web Mercator (EPSG:3857) Not rated or not available -Local Roads Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts Soil Rating Lines Background distance and area. A projection that preserves area, such as the Aerial Photography Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required. This product is generated from the USDA-NRCS certified data as of the version date(s) listed below. B/D Soil Survey Area: Ocean County, New Jersey Survey Area Data: Version 18, Jun 1, 2020 Soil map units are labeled (as space allows) for map scales 1:50.000 or larger. Not rated or not available Date(s) aerial images were photographed: Jun 26, 2019—Jun 29. 2019 **Soil Rating Points** The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background A/D imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident. B/D

#### **Hydrologic Soil Group**

Map unit symbol	Map unit name	Rating	Acres in AOI	Percent of AOI
EveB	Evesboro sand, 0 to 5 percent slopes	А	0.9	100.0%
Totals for Area of Intere	est		0.9	100.0%

#### **Description**

Hydrologic soil groups are based on estimates of runoff potential. Soils are assigned to one of four groups according to the rate of water infiltration when the soils are not protected by vegetation, are thoroughly wet, and receive precipitation from long-duration storms.

The soils in the United States are assigned to four groups (A, B, C, and D) and three dual classes (A/D, B/D, and C/D). The groups are defined as follows:

Group A. Soils having a high infiltration rate (low runoff potential) when thoroughly wet. These consist mainly of deep, well drained to excessively drained sands or gravelly sands. These soils have a high rate of water transmission.

Group B. Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

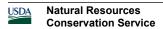
Group C. Soils having a slow infiltration rate when thoroughly wet. These consist chiefly of soils having a layer that impedes the downward movement of water or soils of moderately fine texture or fine texture. These soils have a slow rate of water transmission.

Group D. Soils having a very slow infiltration rate (high runoff potential) when thoroughly wet. These consist chiefly of clays that have a high shrink-swell potential, soils that have a high water table, soils that have a claypan or clay layer at or near the surface, and soils that are shallow over nearly impervious material. These soils have a very slow rate of water transmission.

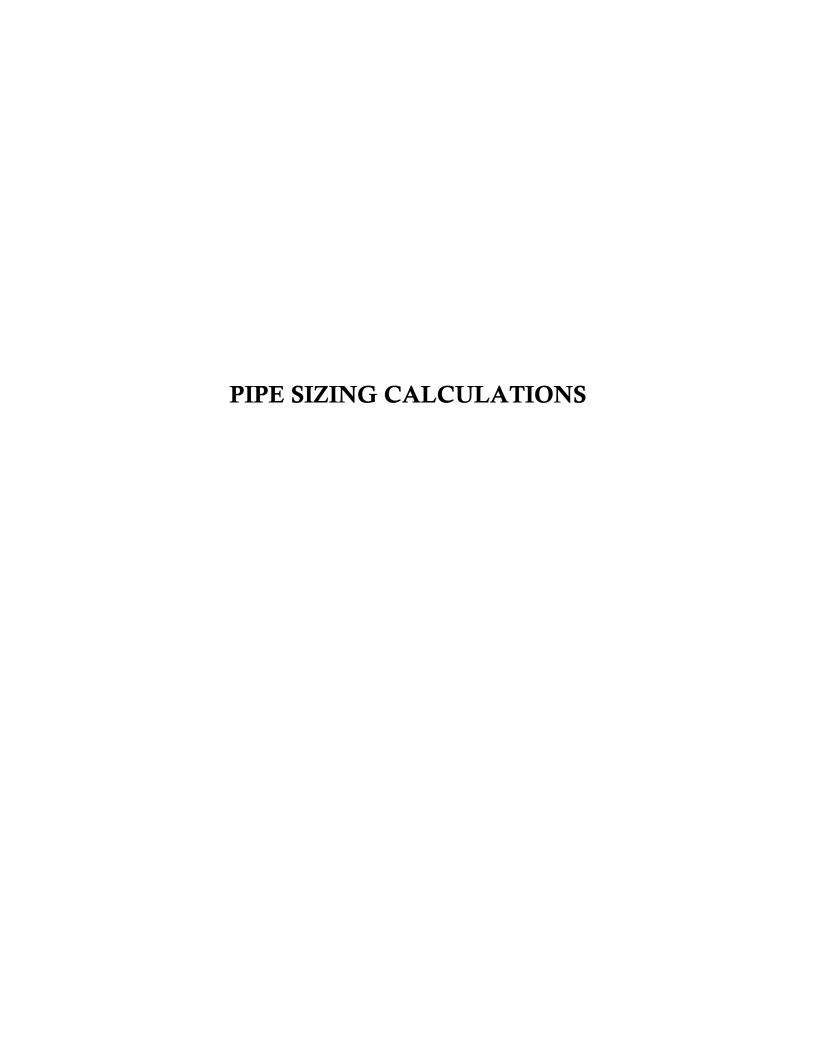
If a soil is assigned to a dual hydrologic group (A/D, B/D, or C/D), the first letter is for drained areas and the second is for undrained areas. Only the soils that in their natural condition are in group D are assigned to dual classes.

#### **Rating Options**

Aggregation Method: Dominant Condition
Component Percent Cutoff: None Specified



Tie-break Rule: Higher





# Inlet Area Summary and Average Coefficient (C) Calculations

Project: NorthStar Capital Computed By: JM Job #: 3639-99-001 Checked By: KK

Location: Borough of Point Pleasant Date: 12/8/2020

Drainage Area	•		•				Total Area (acres)
	Alea (SI)	(O) Oseu	ioi soii sioup B (si )	(O) Oseu	(O) Osed	(51)	(acres)
ROOF	4105	0.95	0		0.95	4105	0.094
ROOF 2	4105	0.95	0		0.95	4105	0.094
Total	8210	0.95	0		0.95	8210	0.188



# **Stormwater Collection System Calculations**Project: NorthStar Capital Computed By: JM

Project: NorthStar Capital Computed By: JM

Job #: 3639-99-001 Checked By: KK

Location: Borough of Point Pleasant Date: 12/8/2020

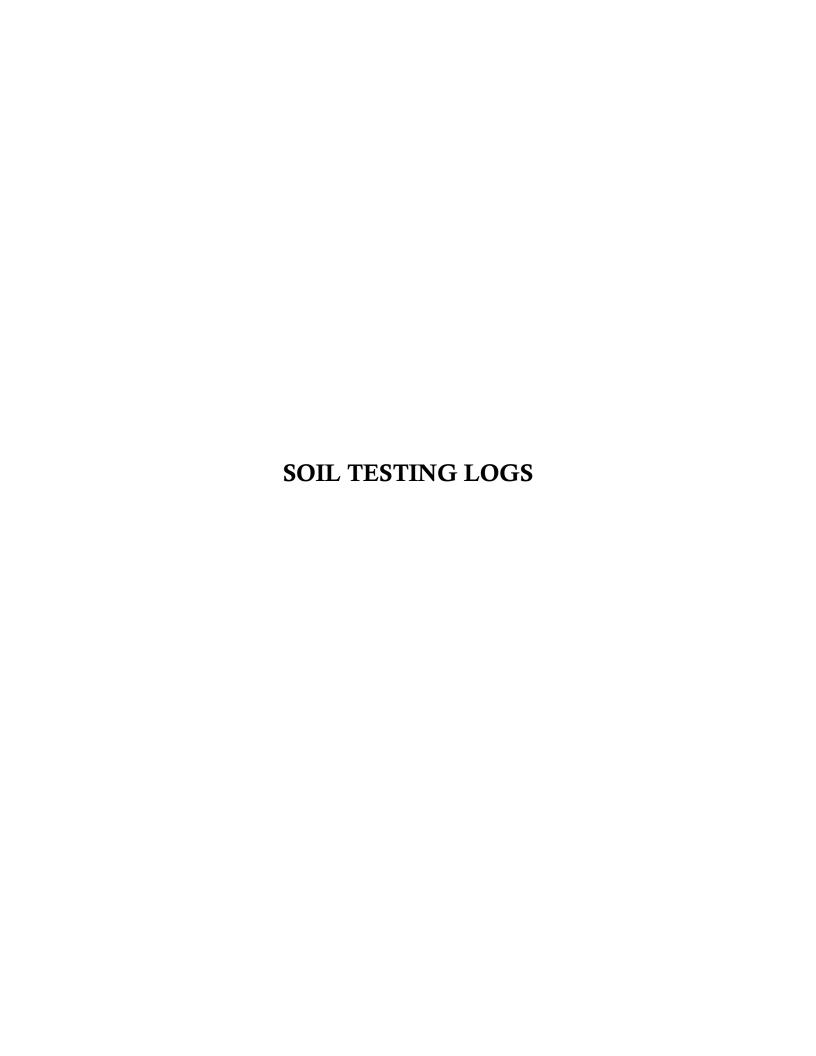
Design Storm: 25 YR

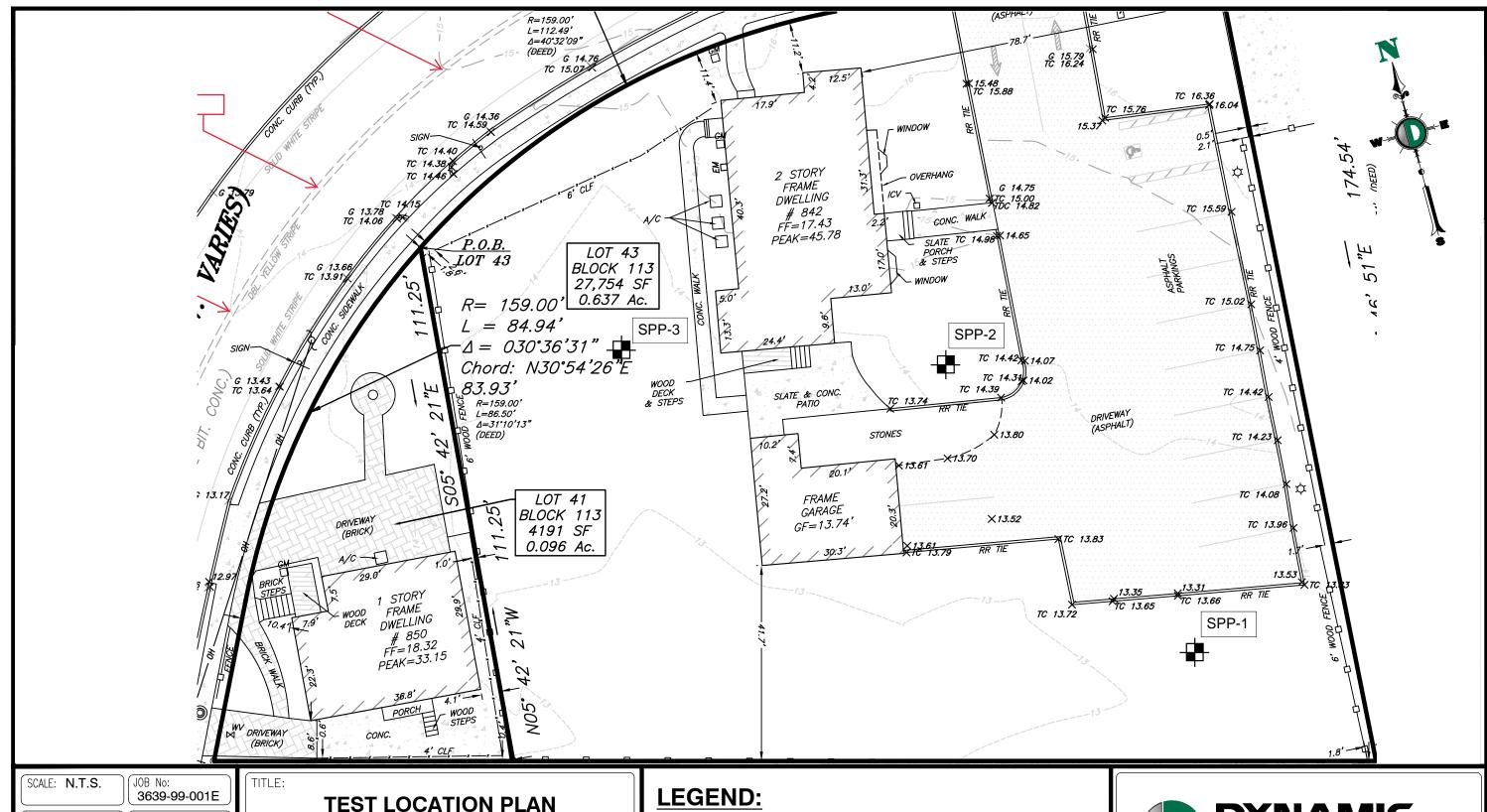
NOTES:

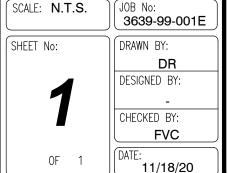
1) Design method used is Rational Method

2) Refer to Weighted Runoff Coefficient table for calculation of incremental areas and C values

PIPE	SECTION	SUBCATCHMENT AREA	INC	REMENTAL	CUMULATIVE		TIME OF CENTRA		Ι	PEAK R	UNOFF	PIF	'ING INP	UT	P	PING DAT	îA
FROM	ТО	Area (Acres)	"C"	AxC Ac	A x C (acres)	Tc to Inlet (min)	Tc in Pipe (min.)	Final Tc (min)	(In/Hr)	Q to Inlet (CFS)	Q cum. for Pipe (CFS)	Dia. (In)	Length (Ft)	Man. "n"	Slope (ft/ft)	Pipe Capacity (cfs)	Pipe Velocity (fps)
ROOF	UG BASIN	0.10	0.95	0.10	0.10	10.00	0.89	10.00	6.80	0.68	0.68	8	169.0	0.010	0.0050	1.11	3.18
ROOF 2	UG BASIN	0.10	0.95	0.10	0.10	10.00	1.11	10.00	6.80	0.68	0.68	8	211.0	0.010	0.0050	1.11	3.18







PROJECT: NORTHSTAR CAPITAL, LLC
PROPOSED MULTI-FAMILY DEVELOPMENT

842 & 850 ARNOLD AVENUE BLOCK 113, LOTS 41 & 43

BOROUGH OF POINT PLEASANT, OCEAN COUNTY NEW JERSEY

Rev. # 0 DEC Client Code: **3639** 



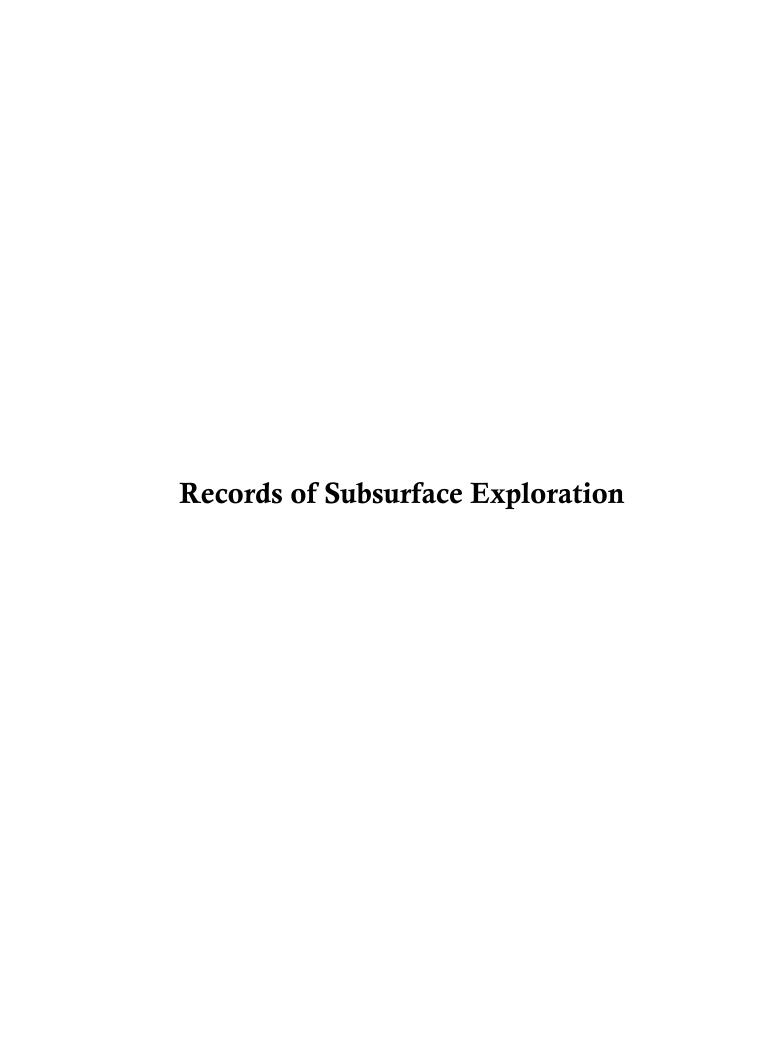
APPROXIMATE LOCATION OF SOIL PROFILE PIT

### NOTES:

- 1. THIS PLAN IS NOT FOR CONSTURCTION AND WAS PREPARED TO ILLUSTRATE TEST LOCATIONS ONLY AND MAY NOT REFLECT THE MOST CURRENT REVISION OF THE BASE PLAN
- 2. THIS PLAN HAS BEEN PREPARED BASED ON A JULY 24, 2020 BOUNDARY & TOPORGRAPHIC SURVEY PREPARED BY INSITE SURVEYING



245 Main Street - Suite 110 Chester, NJ 07930 T: 908.879.7095 - F: 908.879.0222 www.dynamic-earth.com





### SOIL PROFILE PIT LOG

Page <u>1</u> of <u>1</u>

Soil Profile Pit: SPP-1

Project:	Proposed Multi-Fa	mily Developm	ent						Project No.:         3639-99-001E           Client:         NorthStar Capital, LLC															
			h of Point Pleasant, C	cean County, Ne	w Jersey		11/17/20			Groundwater Data Depth EL														
Surface Ele		13.4 9.3	Date Started:				11/17/20		Groundwate	ter Data										Groun	dwater Com	ments		
	n Depth (ft):	9.3 SWM	Date Completed:				Richardson						(ft) NE			(msl	1							
Proposed L Excavation		SWW		Logged by Contractor	<i>/</i> :		nyweight LLC		Seepage Groundwater				NE NE					ł						
/ Test	Visual Observation	1					ASE 580L						NE											
Method:	I			Rig Type	ž:				Seasonal High Groun	indwater														
DEPTH (IN	) COLOR	80	DIL TEXTURE		COARSE FRA	AGMENTS (%	١		STRUCTURE		WATER		CONSISTENCY		BOUN	DARY	ROOTS		MOTTLING			SAMPLING	•	LAB RESULTS
DE1 111 (III	, GOLON		AL TEXTORE		OOALOE 110	NOME INTO (70	,	Shape	Grade	Size	CONTENT	Resistance to Rupture	Stickiness	Plasticity	Distinctness	Topography	Roote	Quantity	Size	Contrast	Туре	Depth (in)	No.	EAD NEGOETO
				GRAVEL	COBBLES	STONES	BOULDERS																	
0 - 14	TOPSOIL Brown (7.5YR 4/2)		LOAM	0	0	0	0	GRANNULAR/ SPHERIODAL	WEAK	MEDIUM	MOIST	VERY FRIABLE	NONSTICKY	NONPLASTIC	CLEAR <2.5"	<b>SMOOTH</b>	CMN (20% COARSE MAX)	NONE			BAG	3	S-1	
				GRAVEL	COBBLES	STONES	BOULDERS	SINGLE GRAIN	STRUCTUR	RELESS														
14 - 37	Dark Yellowish Brown (10YR 4/6)		SAND	<5	0	0	0				MOIST	LOOSE	NONSTICKY	NONPLASTIC	CLEAR <2.5"	WAVY	FEW (5% MAX) MEDIUM	NONE			BAG	20	S-2	
				GRAVEL	COBBLES	STONES	BOULDERS	SINGLE GRAIN	STRUCTUR	RELESS														
37 - 111	Yellowish Brown (10YR 5/6)		SAND	<5	0	0	0				MOIST	LOOSE	NONSTICKY	NONPLASTIC			NONE	NONE			BAG TUBE	80	S-3 T-1	A > 20 iph B > 20 iph
								-																
								_																
Additiona	Remarks: SPP	1 was termin	ated approximately	rat 9.3 feet he	low around s	urface due	to continous d	ry cave-in																



#### SOIL PROFILE PIT LOG

Soil Profile Pit: SPP- 2
Page 1 of 1

roject:	Proposed Multi-Fami 842 & 850 Arnold Ave													3639-99-001E NorthStar Capital,	LLC									
Surface Elev			Journy, Nev					C	nator Data			Depth			El.					· · · · ·	iwater Comn	t-		
Termination		8.3 Date Completed:				11/17/20		Groundy	vater Data			(ft)			(msl)					Ground	iwater Comn	ients		
Proposed Lo Excavation	cation:	SWM	Logged by			Richardson		Seepage				NE			-									
/ Test	Visual Observation		Contractor:			nyweight LLC		Groundwater				NE												
Method:			Rig Type	:	C	ASE 580L		Seasonal High Gr	oundwater			NE			-									
DEPTH (IN)	COLOR	SOIL TEXTURE		COARSE FRA	CMENTS (%)			STRUCTURE		WATER		CONSISTENCY		BOUN	IDARY	ROOT	re		MOTTLING		:	SAMPLING		LAB RESULTS
DE1 111 (IIV)	OGEGIN	OOL TEXTORE		OUNIOE I IO	tomento (A)	'	Shape	Grade	Size	CONTENT	Resistance to Rupture	Stickiness	Plasticity	Distinctness	Topography			Quantity	Size	Contrast	Туре	Depth (in)	No.	LAD NEGOETO
			GRAVEL	COBBLES	STONES	BOULDERS																		
0 - 6	TOPSOIL Brown (7.5YR 4/2)	LOAM	0	0	0	0	GRANNULAR/ SPHERIODAL	WEAK	MEDIUM	MOIST	VERY FRIABLE	NONSTICKY	NONPLASTIC	CLEAR <2.5"	SMOOTH	CMN (20% MAX)	VERY FINE	NONE			BAG	3	S-1	
			GRAVEL	COBBLES	STONES	BOULDERS	SINGLE GRAIN	STRUCT	URELESS															
6 - 50	Dark Yellowish Brown (10YR 4/6)	LOAMY SAND	<5	0	0	0				MOIST	LOOSE	NONSTICKY	SLIGHTLY PLASTIC	CLEAR <2.5"	WAVY	NONE		NONE			BAG TUBE	24 40	S-2 T-1	
			GRAVEL	COBBLES	STONES	BOULDERS	SINGLE GRAIN	STRUCT	URELESS															
50 - 100	Yellowish Brown (10YR 5/6)	SAND	<5	0	0	0	-			MOIST	LOOSE	NONSTICKY	NONPLASTIC			NONE		NONE			BAG TUBE	100	S-3 T-2	A > 20 lph B > 20 lph
							-																	
Additional	Remarks: SPP-2	was terminated approximately a	t 8.3 feet bel	ow ground su	urface due t	o continous di	y cave-in.														l			



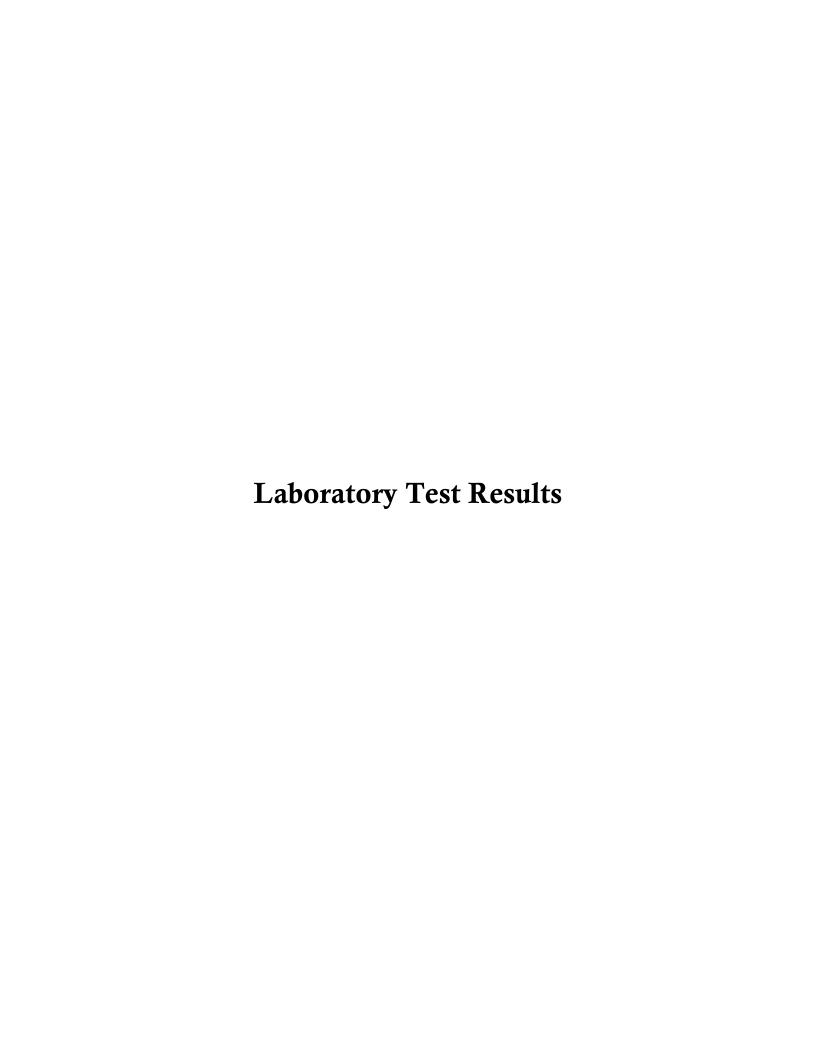
#### SOIL PROFILE PIT LOG

Page <u>1</u> of <u>1</u>

Soil Profile Pit: SPP-3

roject:	Proposed Multi-Family	y Development									Project No.:			3639-99-001E									
ocation: urface Elevi		nue, Borough of Point Pleasant, 6 13.4 Date Started:	cean County, N	w Jersey		11/17/20		I		1	Client:	Depth		NorthStar Capital,	EL.								
ermination I		8.0 Date Completed				11/17/20		Groundw	vater Data			(ft)			(msl)				Ground	water Comm	ents		
roposed Lo	cation:	SWM	Logged b			. Richardson		Seepage				NE			-								
xcavation / Test	Visual Observation		Contracto			nyweight LLC		Groundwater				NE					4						
Method:			Rig Typ	e:		CASE 580L		Seasonal High Gro	oundwater			NE			-								
DEPTH (IN)	COLOR	SOIL TEXTURE		COARSE ER	AGMENTS (%	a		STRUCTURE		WATER		CONSISTENCY		BOUN	DARY	ROOTS		MOTTLING		s	SAMPLING		LAB RESULTS
						,	Shape	Grade	Size	CONTENT	Resistance to Rupture	Stickiness	Plasticity	Distinctness	Topography		Quantity	Size	Contrast	Type	Depth (in)	No.	
			GRAVEL	COBBLES	STONES	BOULDERS																	
0 - 12	TOPSOIL Brown (7.5YR 4/2)	LOAM	0	0	0	0	GRANNULAR/ SPHERIODAL	WEAK	MEDIUM	MOIST	VERY FRIABLE	NONSTICKY	NONPLASTIC	CLEAR <2.5"	SMOOTH	CMN (20% VERY MAX) FINE	NONE			BAG	3	S-1	
			GRAVEL	COBBLES	STONES	BOULDERS	SINGLE GRAIN	STRUCTI	URELESS														
12 - 51	Dark Yellowish Brown (10YR 4/6)	LOAMY SAND	<5	0	0	0				MOIST	LOOSE	NONSTICKY	SLIGHTLY PLASTIC	CLEAR <2.5"	WAVY	NONE	NONE			BAG TUBE	38	S-2 T-1	
			GRAVEL	COBBLES	STONES	BOULDERS	SINGLE GRAIN	STRUCTI	URELESS														
51 - 96	Yellowish Brown (10YR 5/6)	SAND	<5	0	0	0				MOIST	LOOSE	NONSTICKY	NONPLASTIC			NONE	NONE			BAG TUBE	90	S-3 T-2	A > 20 iph B > 20 iph
							1									1				1		1	

Additional Remarks: Debris encountered approximately at 8.0 feet below dreund surface. Debris included brick. SPP-3 was terminated approximately at 8.0 feet below ground surface due to continous dry cave-in.



Job Number: 3639-99-001E
Project: Proposed Residual Building

Sample ID:	Boring/T	est Pit No.:	1 Sam	ple No.:	1	Depth:	6.7 ft	Client: NorthStar Capital
MUNICIPALI	ITY	Point Pleasa	ant	BLOCK	113	LOT	41&43	Lab Tech: Sam
1. Test Numb	ber	1	Replicate (letter)	A	_Date Colle	ected	11/18/2020	
2. Material T	ested:		Fill X	Test in N	ative Soil-Ind	dicate Depth		
3. Type of S	ample:	x	Undisturbed		_Disturbed			
4. Sample D	imensions:		Inside Radius of Sar Length of Sample, L		R, in cm	1.905 3.50		
5. Bulk Dens	sity Determi	nation (Distur	bed Samples Only):	N/A				
6. Sample W	Veight (Wt. 7	Гube Contain	ing Sample-Wt. of Er	mpty Tube),	grams			Wt. of Tube Containing Sample Wt. of Empty Tube
7. Sample V	olume (L x 2	2.54 cm./inch	x 3.14R2), cc.			101.3028		
8. Bulk Dens	sity (Sample	Wt./Sample	Volume), grams/cc.				> 1.2	
9. Standpipe	e Used:	х	No	Yes, Indi	cate Interna	l Radius, cm	. N/A	
10. Height of	f Water Lev	el Above Rim	of Test Basin, in inc	hes:				
		inning of Eac of Each Test	h Test Interval, H1 t Interval, H2	5.50 4.50				
11. Rate of V	Water Level	Drop (Add a	dditional lines if need	led):				
		art of Test erval, T1	Time End of Test Interval T2		h of Test T, Minutes			
	0:0	00:00	0:00:29	С	).49			
	0:0	00:00	0:00:25	C	).42			
	0:0	00:00	0:00:25	C	).42			
12. Calculati	ion of Perme	eability:	K, (in/hr) = 60 min/h	r x r2/R2 x L(	(in)/T(min) x	J In (H1/H2)	T= <u>0.4</u>	12
	K =	> 20	Classific	cation:	K5			
13. Defects i	in the Samp	le (Check ap	propriate items):					
	X	NONE						
		Soil/Tube Co	ntactLarg	e Gravel		_ Large Roo	ts	
		Dry Soil	Smearing		Compac	tion		
		Other - Spec	ify					

\_\_\_\_\_ Soil/Tube Contact \_\_\_\_\_Large Gravel \_\_\_\_\_ Large Roots \_\_\_\_ Dry Soil \_\_\_\_\_Smearing \_\_\_\_ Compaction

\_\_\_ Other - Specify \_\_\_

**Tube Permeameter Test Data** Job Number: 3639-99-001E Project: Proposed Residual Building Sample ID Boring/Test Pit No.: 1 Sample No.: 1 Depth: 6.7 ft Client: NorthStar Capital Lab Tech: Sam MUNICIPALITY Point Pleasant **BLOCK** 113 LOT 41&43 B Date Collected 2 Replicate (letter) 11/18/2020 1. Test Number 2. Material Tested: Fill \_\_\_\_X \_\_\_ Test in Native Soil-Indicate Depth x Undisturbed 3. Type of Sample: Disturbed 4. Sample Dimensions: Inside Radius of Sample Tube, R, in cm Length of Sample, L, in inches 5. Bulk Density Determination (Disturbed Samples Only): N/A 6. Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams Wt. of Tube Containing Sample Wt. of Empty Tube 108.5387 7. Sample Volume (L x 2.54 cm./inch x 3.14R2), cc. 8. Bulk Density (Sample Wt./Sample Volume), grams/cc. > 1.2 Yes, Indicate Internal Radius, cm. N/A 9. Standpipe Used: x No 10. Height of Water Level Above Rim of Test Basin, in inches: At the Beginning of Each Test Interval, H1 At the End of Each Test Interval, H2 11. Rate of Water Level Drop (Add additional lines if needed): Time, Start of Test Time End of Test Length of Test Interval, T1 Interval T2 Interval, T, Minutes 0:00:00 0:00:22 0.37 0:00:21 0.36 0:00:00 0:00:00 0:00:27 0.45 12. Calculation of Permeability: K, (in/hr) = 60 min/hr x r2/R2 x L(in)/T(min) x ln (H1/H2) T= 0.45 Classification: > 20 13. Defects in the Sample (Check appropriate items): \_\_\_x\_\_NONE

**Job Number:** 3639-99-001E Project: Proposed Residual Building
Client: NorthStar Capital

Sample ID Bo	ring/Test Pit No.:	2 Sampl	e No.: 2	Depth:	8.3 ft	Project: Proposed Residual Building Client: NorthStar Capital
MUNICIPALITY	Point Pleas	ant	BLOCK 113	LOT	41&43	Lab Tech: Sam
1. Test Number	r <u>2</u>	Replicate (letter)	ADate Col	llected	11/18/2020	
2. Material Tes	sted:	Fill X	Test in Native Soil-I	Indicate Depth	1	
3. Type of San	nple: x	Undisturbed	Disturbed	d		
4. Sample Dim		Inside Radius of Samp Length of Sample, L, i		1.905 3.50		
5. Bulk Density	y Determination (Di	sturbed Samples Only)	): N/A			
6. Sample Wei	ight (Wt. Tube Cont	taining Sample-Wt. of I	Empty Tube), grams		•	Wt. of Tube Containing Sample Wt. of Empty Tube
7. Sample Volu	ume (L x 2.54 cm./i	nch x 3.14R2), cc.		101.3028	•	W. of Empty Tube
8. Bulk Density	y (Sample Wt./Sam	ple Volume), grams/cc			> 1.2	
9. Standpipe U	Jsed: x	No	Yes, Indicate Interr	nal Radius, cm	n. N/A	
10. Height of V	Vater Level Above	Rim of Test Basin, in ir	nches:			
	he Beginning of Ea he End of Each Tes	ch Test Interval, H1 st Interval, H2	5.50 4.50			
11. Rate of Wa	ater Level Drop (Ad	d additional lines if nee	eded):			
Ti	me, Start of Test Interval, T1	Time End of Test Interval T2	Length of Test Interval, T, Minutes	S		
	0:00:00	00:34.9	0.58			
	0:00:00	00:38.0	0.63			
	0:00:00	0:00:31	0.52			
12. Calculation	of Permeability:	K, (in/hr) = 60 min/hr x	r2/R2 x L(in)/T(min)	x In (H1/H2)	T= 0.5	2
K =	> 20	Classifica	tion: K5			
13. Defects in	the Sample (Check	appropriate items):				
	x NONE					
	Soil/Tube C	ontactLarge	Gravel	Large Ro	oots	
	Dry Soil	Smearing _	Comp	paction		
	Other - Spe	cify				

\_\_\_\_\_ Soil/Tube Contact \_\_\_\_\_Large Gravel \_\_\_\_\_ Large Roots \_\_\_\_ Dry Soil \_\_\_\_\_Smearing \_\_\_\_ Compaction

\_\_ Other - Specify \_\_\_

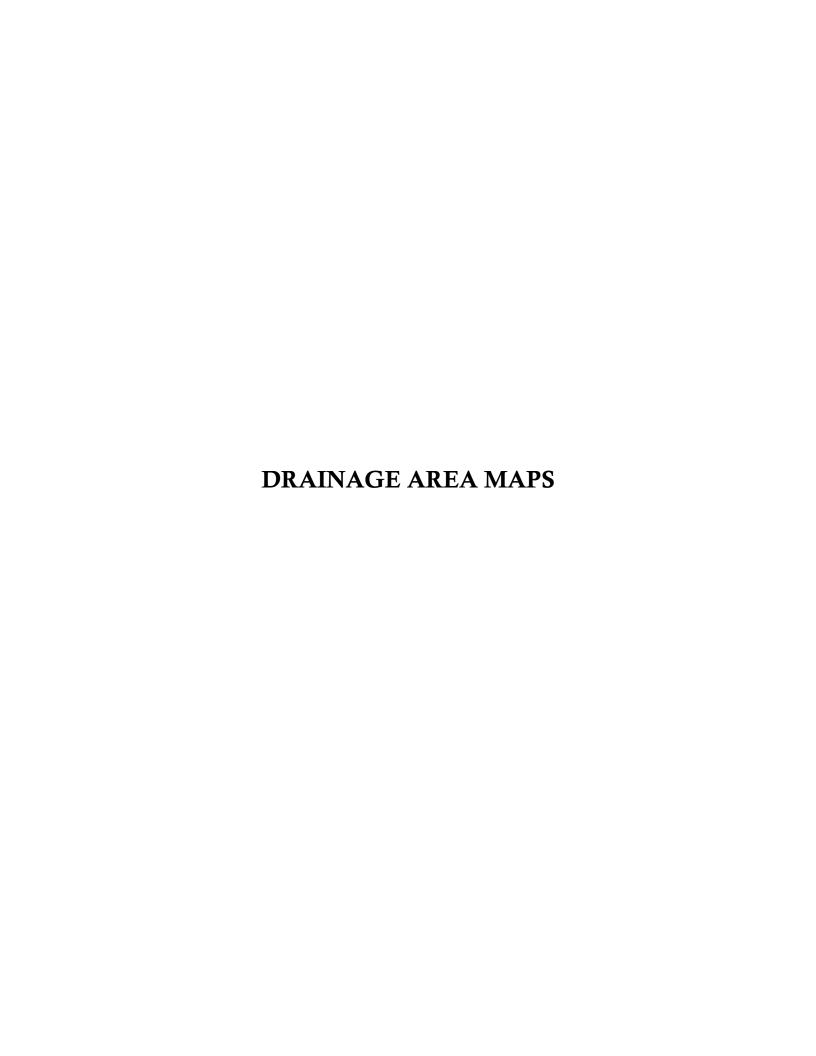
Job Number: 3639-99-001E Project: Proposed Residual Building Sample ID Boring/Test Pit No.: 2 Sample No.: 2 Depth: 8.3 ft Client: NorthStar Capital Lab Tech: Sam MUNICIPALITY Point Pleasant **BLOCK** 113 LOT 41&43 B Date Collected 2 Replicate (letter) 11/18/2020 1. Test Number X Test in Native Soil-Indicate Depth 2. Material Tested: Fill x Undisturbed 3. Type of Sample: Disturbed 4. Sample Dimensions: Inside Radius of Sample Tube, R, in cm Length of Sample, L, in inches 5. Bulk Density Determination (Disturbed Samples Only): N/A 6. Sample Weight (Wt. Tube Containing Sample-Wt. of Empty Tube), grams Wt. of Tube Containing Sample Wt. of Empty Tube 101.3028 7. Sample Volume (L x 2.54 cm./inch x 3.14R2), cc. 8. Bulk Density (Sample Wt./Sample Volume), grams/cc. > 1.2 Yes, Indicate Internal Radius, cm. N/A 9. Standpipe Used: x No 10. Height of Water Level Above Rim of Test Basin, in inches: At the Beginning of Each Test Interval, H1 At the End of Each Test Interval, H2 11. Rate of Water Level Drop (Add additional lines if needed): Time, Start of Test Time End of Test Length of Test Interval, T1 Interval T2 Interval, T, Minutes 0:00:00 00:42.0 0.70 00:43.0 0.72 0:00:00 0:00:00 0:00:40 0.67 12. Calculation of Permeability: K, (in/hr) = 60 min/hr x  $r2/R2 \times L(in)/T(min) \times ln (H1/H2)$  T= 0.67 Classification: > 20 K5 13. Defects in the Sample (Check appropriate items): \_\_\_x\_\_NONE

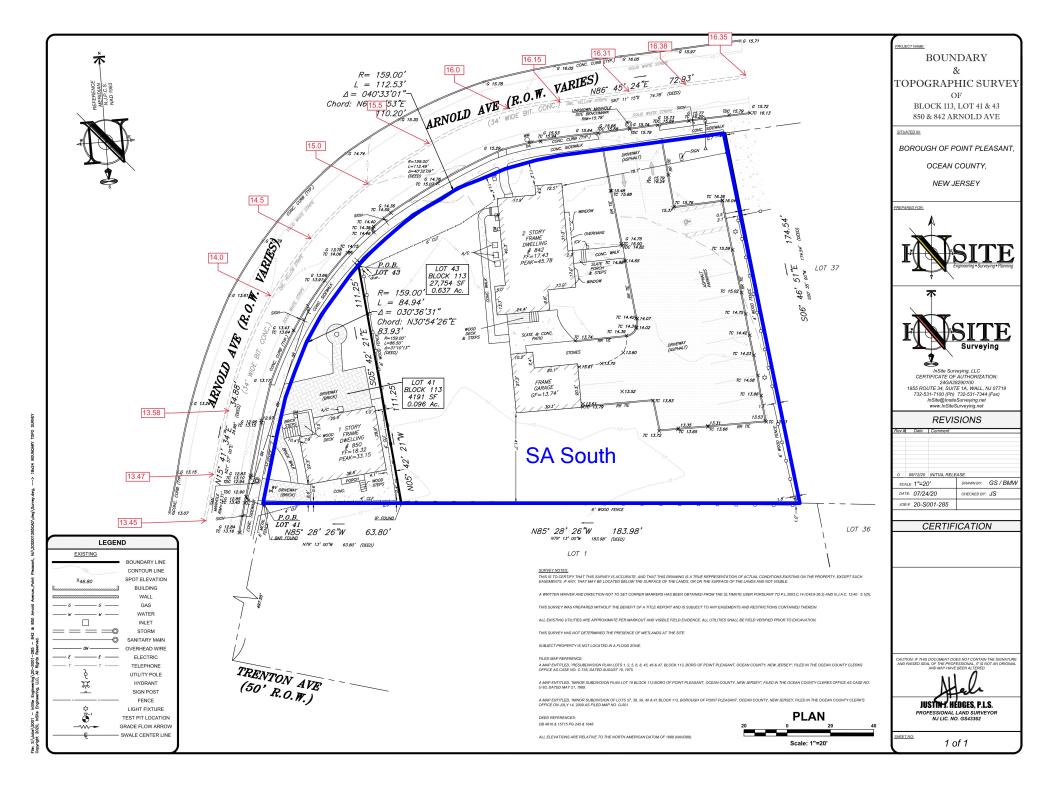
Job Number: 3639-99-001E Project: Proposed Residual Building Client: NorthStar Capital

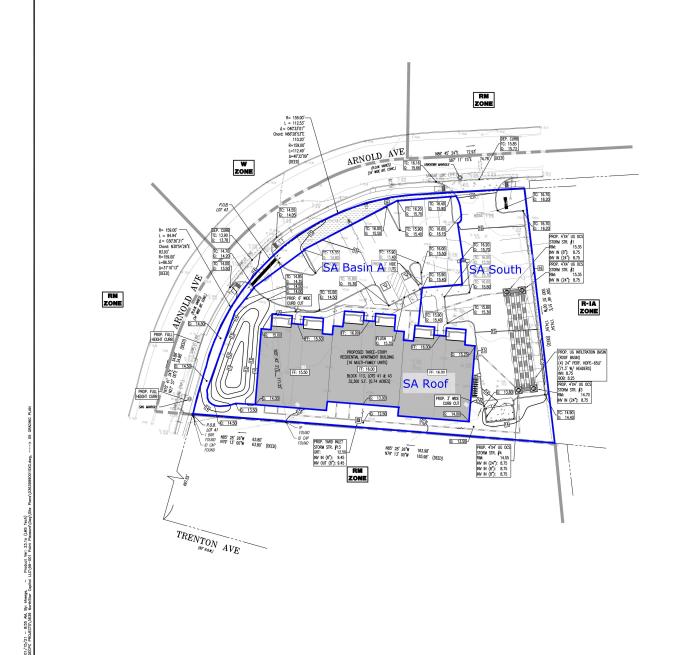
Sample ID	Boring/Te	est Pit No.:	3	Sample	e No.:	2	Depth:	7.5 ft	Client: NorthStar Capital Lab Tech: Sam
MUNICIPAL	LITY	Point Pleas	sant		BLOCK	113	_LOT	41&43	Lab rech. Sam
1. Test Num	nber	1	Replicate (le	tter)	Α	_ Date Colle	ected	11/18/2020	
2. Material	Tested:		Fill _	Х	Test in Na	ative Soil-Ir	ndicate Depth		
3. Type of S	Sample:	Х	Undisturbed	-		Disturbed	I		
4. Sample [	Dimension		Inside Radiu Length of Sa			R, in cm	1.905 3.50		
5. Bulk Den	nsity Deterr	mination (Di	sturbed Sam	ples Only)	: N/A				
6. Sample V	Weight (Wt	t. Tube Con	taining Samp	le-Wt. of E	mpty Tube	e), grams			Wt. of Tube Containing Sample Wt. of Empty Tube
7. Sample \	Volume (L	x 2.54 cm./i	inch x 3.14R2	!), cc.			101.3028		
8. Bulk Den	nsity (Samp	ole Wt./Sam	iple Volume),	grams/cc.				> 1.2	
9. Standpip	e Used:	Х	No _		Yes, Indi	icate Interna	al Radius, cm	. N/A	
10. Height of	of Water Le	evel Above	Rim of Test E	Basin, in in	ches:				
			ich Test Interv st Interval, H2		5.50 4.50				
11. Rate of	Water Lev	vel Drop (Ad	ld additional li	nes if nee	ded):				
		art of Test rval, T1	Time End Interva			h of Test T, Minutes			
	0:00	0:00	00:44	.5	0	).74			
	0:00	0:00	00:47	'.2	0	).79			
	0:00	0:00	0:00:	52	0	).87			
12. Calculat	tion of Per	meability:	K, (in/hr) = 6	0 min/hr x	r2/R2 x L(	(in)/T(min) x	k In (H1/H2)	T= <u>0.8</u>	7
ŀ	K =	> 20		lassificat	ion:	K5			
13. Defects	in the San	mple (Check	appropriate	items):					
_	х	NONE							
-	:	Soil/Tube C	ontact	Large	Gravel _		Large Ro	ots	
-	!	Dry Soil	Sı	mearing _		Compa	action		
-		Other - Spe	cify						

Job Number: 3639-99-001E Project: Proposed Residual Building Client: NorthStar Capital

Sample ID Boring/	Test Pit No.:	3 <b>S</b>	ample No.:	2	Depth:	7.5 ft	Client: NorthStar Capital  Lab Tech: Sam
MUNICIPALITY	Point Plea	sant	BLOCK	113	_LOT _	41&43	Lab Tech: Sam
1. Test Number	2	Replicate (letter)	В	_Date Col	lected _	11/18/2020	
2. Material Tested:		Fill X	Test in N	ative Soil-I	ndicate Depth		
3. Type of Sample:	x	Undisturbed		_ Disturbed	d		
4. Sample Dimension	ons:	Inside Radius of Sample		R, in cm	1.905 4.00		
5. Bulk Density Dete	ermination (D	isturbed Samples	Only): N/A				
6. Sample Weight (\	Wt. Tube Cor	ntaining Sample-W	t. of Empty Tube	e), grams			Wt. of Tube Containing Sample Wt. of Empty Tube
7. Sample Volume (	L x 2.54 cm./	inch x 3.14R2), cc			115.7746		
8. Bulk Density (Sar	mple Wt./San	nple Volume), gran	ns/cc.			> 1.2	
9. Standpipe Used:	x	No	Yes, Indi	icate Intern	nal Radius, cm.	N/A	
10. Height of Water	Level Above	Rim of Test Basin	, in inches:				
		ach Test Interval, F est Interval, H2	5.00				
11. Rate of Water Lo	evel Drop (Ad	dd additional lines	f needed):				
	Start of Test terval, T1	Time End of Te Interval T2		h of Test T, Minutes	5		
0:	:00:00	00:37.1	0	0.62			
0:	:00:00	00:35.9	0	0.60			
0:	:00:00	0:00:40	O	0.66			
12. Calculation of Po	ermeability:	K, (in/hr) = 60 mir	n/hr x r2/R2 x L(	(in)/T(min)	x In (H1/H2)	T= 0.66	<u> </u>
K =	> 20	Class	ification:	K5			
13. Defects in the S	ample (Chec	k appropriate item	s):				
X	NONE						
	_ Soil/Tube C	ContactL	arge Gravel _		Large Roc	ots	
	_ Dry Soil	Smear	ing	Comp	action		
	_ Other - Spe	ecify					







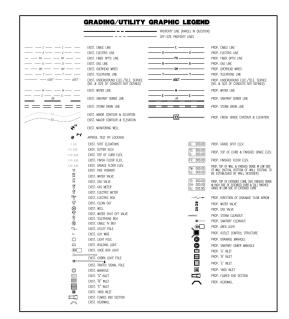


2. CONTRACTOR IS RESPONSIBLE FOR VERRICATION OF DISTING TOPOSPHAPE INFORMATION AND UTILITY INVEST ELERATIONS PROCE TO COMMENCED IN THE AUGUST ALL TOPOSPHAPE IN TOPOSPHAPE IN THE AUGUST AUG

- PROPOSED TOP OF CURB PLENTONS ARE CONSTALLY 6" ARXIV EXISTING LOCAL ASPHALT ORDIC UNLESS OTHERWISE NOTED. FIELD ADJUST TO ORBITE A MIN. OF 0.75% GUTTER GRADE ALDING CURB FACE, ENJANCER TO APPRING FINAL CURBING OUT SPEEDS PRIOR TO INSTALLATION. 4. SUBBASE MUTERAL FOR SIDEMAKS, DURB, OR ASPHALT SHALL BE FREE OF ORDANDS AND OTHER UNSURINKE MUTERALS. SHOULD SUBBASE BE DEEMED UNSURINKE, SUBBASE IS TO BE REMOVED AND FILED WITH APPROVED FILL MATERAL COMPACTED TO 90% OPTIMUM DENSITY (AS DETERMINED BY MODIFED PROCISIO WHENDO.)
- 6. IN CASE OF DISCREPANCIES BETWEEN PLANS, THE SITE PLAN WILL SUPERCEDE IN ALL CASES. CONTRACTOR WIST NOTIFY ENGINEER OF RECORD OF ANY CONFLICT IMPERATELY.
- 7. MAXIMUM CROSS SLOPE OF 2% ON ALL SIDEMALKS.

w-(D

- 8. CONTRACTOR TO ENSURE A MAXIMUM OF 25 SLOPE IN ALL DIRECTIONS IN JOA PAPKING SPACES AND AGA ACCESS ASLES. CONTRACTOR TO EXISTRE A MAXIMUM OF 35 SHOWNED, THE AMOUNT OF A PAPKING SPACES AND AGA ACCESS ASLES. CONTRACTOR IN AN OLD THE AMOUNT OF A PAPKING SPACES AND AGA ACCESS ASLES. CONTRACTOR OF A PAPKING SPACES AND AGA ACCESS ASLES. CONTRACTOR AND SPACES AND AGA ACCESS ASLES. CONTRACTOR AND SPACES AND AGA ACCESS ASLES. CONTRACTOR AND AGA ACCESS ASLES. CONTRACTOR AND AGA ACCESS ASLES. CONTRACTOR AND AGA ACCESS ASLES. CONTRACTOR AND AGA ACCESS ASLES. CONTRACTOR AND ACCESS ASLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR AND AGA ACCESS ASSLES. CONTRACTOR ASSLES. CONTRACTOR ASSLESS A
- 9. THE CONNER SHALL RETAIN DINNANC EARTH, LLC (908-839-7025) OR AUTEMATE QUALIFIED DEDIED-INCAL ENGINEER TO TEST SOIL PRINCE/BUILTY AND PROVIDE CONSTRUCTION PRICE RESPECTIONS OF THE BISIN BOTTON SOILS AND ANY FILL MATERIALS WITHIN ANY PROPERCED INFLITIATION OR RETENTION BISIN TO COMPRISE RESULTS TO LEGACION CONTENT.
- 10. CONTRACTOR IS TO REMOVE EXISTING UNSUITABLE OR OVERLY COMPACT SOIL OR ROCK AS NEEDED TO ACHEVE REQUIRED PERMEABILITY AS DIRECTED BY THE OWNERS CEDITECHNICAL ENGINEER, AND MEN FILL, IF METERD, SHALL HAVE AN IN PLACE PERMEABILITY GREATER THAN OR COLUM, TO THE DESIGN CONTENA. 11. CONTRACTOR IS RESPONSIBLE FOR CONDUCTING THE OWNER'S GEOTECHNICAL ENGINEER PRIOR TO CROSET OF CONSTRUCTION TO SUBMIT AND CONFIRM THE CONTRACTOR'S PROPOSED BANKS AND MATERIALS AND TO SCHEDULE INSPECTIONS FOR BOTTOM OF BASIN, REMOVE, OF UNSURNEE SOL, PLL PLACEMENT, AND PARK LISES PRESIDENT TESTING.





tvis plad set is for permitting purposes only and may not be used for construct DYNAMIC ENGINEERING GRADING PLAN NORTHSTAR CAPITAL, LLC 3639-99-001 DRAWN BY: KJH PROPOSED MULTI-FAMILY RESIDENTS (POINT VIEW LUXURY APARTMENTS) SCALE: (H) 1"=20 DESIGNED BY: KCK SHEET No. CHECKED RY: 5 DOUGLAS GRYSKO KYLE C. KAVINSKI PROTECT YOURSELF

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